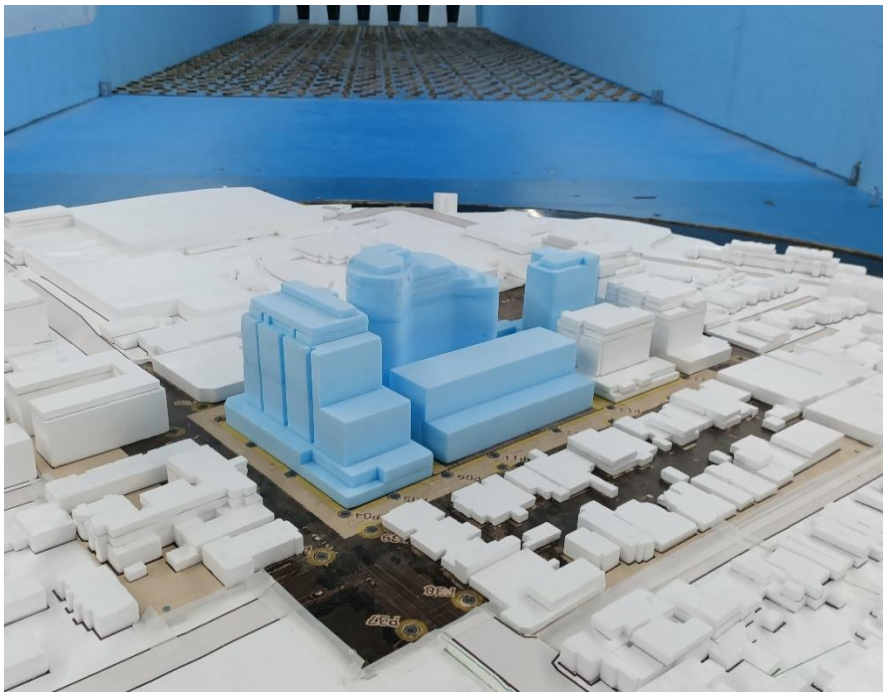

PEDESTRIAN WIND ENVIRONMENT STUDY

81-95 BURNLEY STREET & 26-34 DOONSIDE STREET, RICHMOND

WG433-04F02(REV3)- WE REPORT

JULY 13, 2023

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DOCUMENT CONTROL

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EXECUTIVE SUMMARY

This report presents the results of a detailed investigation into the wind environment impact of the masterplan of the 81-95 Burnley Street development, located in Richmond, Victoria. Testing was performed at Windtech's boundary layer wind tunnel facility. The wind tunnel has a 3.0m wide working section and a fetch length of 14m, and measurements were taken from 16 wind directions at 22.5 degree increments. Testing was carried out using a 1:300 scale model of the development massing. The effects of nearby buildings and land topography have been accounted for through the use of a proximity model which represents an area with a radius of 375m.

Peak gust and mean wind speeds were determined at selected critical outdoor trafficable locations within and around the subject development site. Wind velocity coefficients representing the local wind speeds are derived from the wind tunnel and are combined with a statistical model of the regional wind climate (which accounts for the directional strength and frequency of occurrence of the prevailing regional winds) to provide the equivalent full-scale wind speeds at the site. The wind speed measurements are compared with criteria for pedestrian comfort and safety, based on Gust-Equivalent Mean (GEM) and annual maximum gust winds, respectively.

The model was tested in the wind tunnel without the effect of any forms of wind ameliorating devices such as screens, balustrades, etc., which are not already shown in the architectural drawings. The effect of vegetation was also excluded from the testing. The existing site conditions were also tested, for comparison.

The results of the study indicate that wind conditions for many trafficable outdoor locations within and around the development will be suitable for their intended uses. Some areas will experience strong winds which will exceed the relevant criteria for safety and/or the existing site conditions. Additional wind tunnel testing was conducted with the inclusion of treatments for these areas. The results of the additional testing indicated the following treatment scheme was effective in wind mitigation and the outdoor trafficable areas within and around the development site will meet the safety limit criterion and/or better than the existing site conditions:

Doonside Park:

- Inclusion of 1-1.5m high raised garden beds along the public open space.
- Strategic inclusion of impermeable screens atop of the raised garden beds, with an overall height of 2.5m from the local ground level.
- Inclusion of a 2.5m high porous screen along the perimeter edge of the proposed paving at the centre of the public open space. The porosity of the screen is to be a maximum of 30%.
- The proposed bench adjacent to the heritage building is to have a 1.5m high impermeable backrest.

Building A:

- Inclusion of impermeable awnings along the northern and western façade of the podium.
- Inclusion of a Level 1 porous canopy along the eastern façade of the podium (between Buildings A and B) with a maximum porosity of 30%.

- Inclusion of fixed openings within the existing ground level windows/door systems at the north-western corner.
- An extension of the proposed north-western lobby entrance further along the southern boundary.
- Inclusion of 1.5m high impermeable balustrades on the Level 2 podium. The impermeable balustrade is to be offset 1.5m away from the podium edge along the northern and western boundaries.
- Inclusion of a north-western corner 4m x 4m wide balcony on all levels of the tower. A full-height porous screen is also to be included along the western perimeter edge of the balconies with a maximum porosity of 30%.

Building B:

- Inclusion of Level 2 impermeable awnings along the northern façade of the podium.
- Inclusion of a Level 2 porous canopy along the eastern façade of the podium with a maximum porosity of 30%.

Building C:

- Inclusion of 3m high impermeable screens along the north-western perimeter edge of the Level 2 podium rooftop.
- Inclusion of a porous canopy atop of the abovementioned 3m high impermeable screen. The porosity of the canopy is to be a maximum of 30%.
- Inclusion of 3m high porous screen along most of the eastern edge of the Level 2 podium rooftop.
- Inclusion of a north-eastern corner 3m x 3m wide balcony on all levels of the tower. A full-height porous screen is also to be included along the eastern perimeter edge of the balconies with a maximum porosity of 30%.

It should be noted that many of these issues are due to funnelling, downwash and corner acceleration effects of the northerly winds and will likely be improved or resolved with the inclusion of the Victoria Gardens development across Doonside Street to the north.

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1 INTRODUCTION

A wind tunnel study has been undertaken to determine wind speeds at selected critical outdoor trafficable areas within and around the subject development. The test procedures followed for this wind tunnel study were based on the guidelines set out in the Australasian Wind Engineering Society Quality Assurance Manual (AWES-QAM-1-2019), ASCE 7-16 (Chapter C31), and CTBUH (2013).

A scale model of the development massing was prepared, including the surrounding buildings and land topography. Testing was performed at Windtech's boundary layer wind tunnel facility. The wind tunnel has a 3.0m wide working section and a fetch length of 14m, and measurements were taken from 16 wind directions at 22.5 degree increments. The wind tunnel was configured to the appropriate boundary layer wind profile for each wind direction. Wind speeds were measured using either Dantec hot-wire probe anemometers or pressure-based wind speed sensors, positioned to monitor wind conditions at critical outdoor trafficable areas of the development.

The massing model was tested in the wind tunnel without the effect of any forms of wind ameliorating devices such as screens, balustrades, etc., which are not already shown in the architectural drawings. The effect of vegetation was also excluded from the testing. The wind speeds measured during testing were combined with a statistical model of the regional wind climate to provide the equivalent full-scale wind speeds at the site. The measured wind speeds were compared against appropriate criteria for pedestrian comfort and safety, and in-principle treatments have been recommended for any area which was exposed to strong winds. These treatments could be in the form of retaining vegetation that is already proposed for the site, or including additional vegetation, screens, awnings, etc. Note however that, in accordance with the AWES Guidelines (2014), only architectural elements or modifications are used to treat winds which represent an exceedance of the existing wind conditions and exceed the safety limit.

2 WIND TUNNEL MODEL

Wind tunnel testing was carried out using a 1:300 scale model of the development massing and surroundings. The massing study model was constructed using a Computer Aided Manufacturing (CAM) process to ensure that a high level of detail and accuracy is achieved. The effect of nearby buildings and land topography has been accounted for through the use of a proximity model, which represents a radius of 375m from the development site. Photographs of the wind tunnel model are presented in Figures 1. A plan of the proximity model is provided in Figure 2.

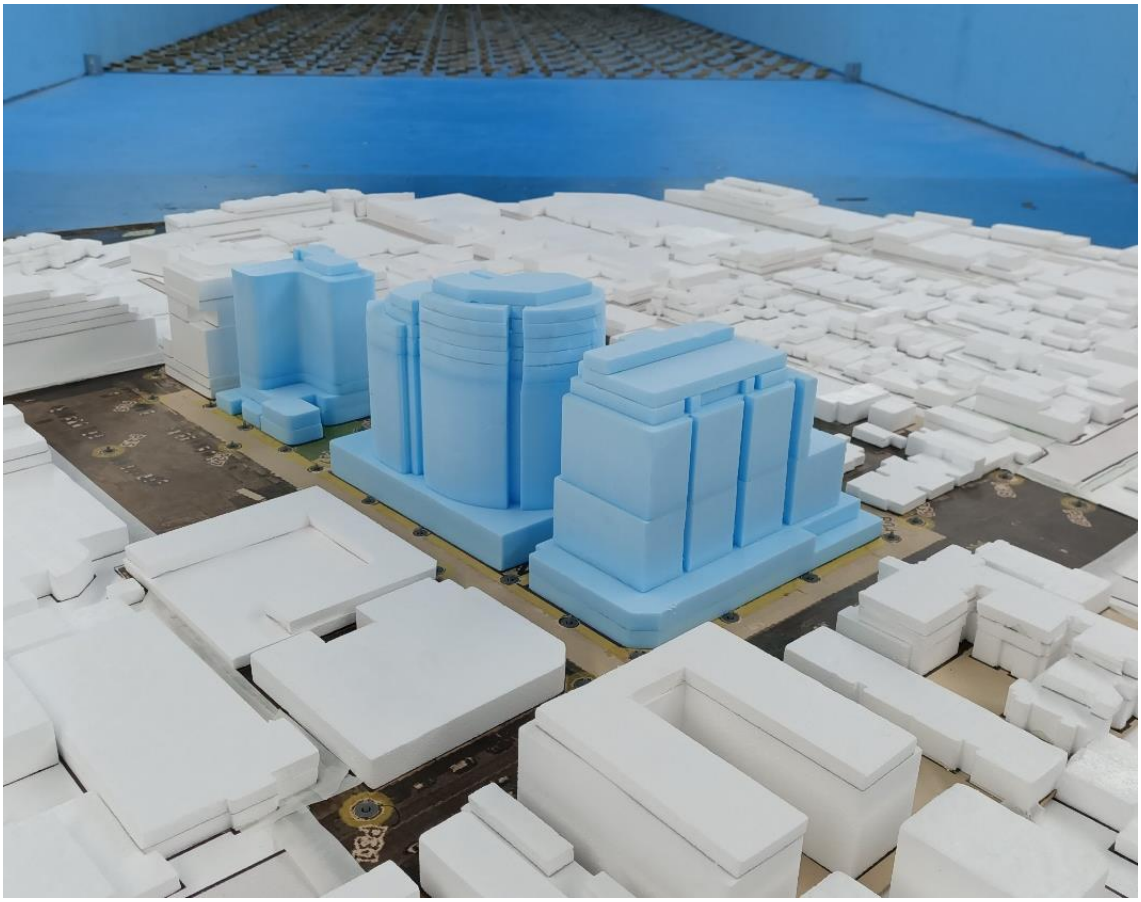


Figure 1a: Photograph of the Wind Tunnel Model (Proposed Site Conditions, view from the north-west)

Figure 1b: Photograph of the Wind Tunnel Model (Proposed Site Conditions, view from the north)

Figure 1c: Photograph of the Wind Tunnel Model (Proposed Site Conditions, view from the east)

Figure 1d: Photograph of the Wind Tunnel Model (Proposed Site Conditions, view from the south)

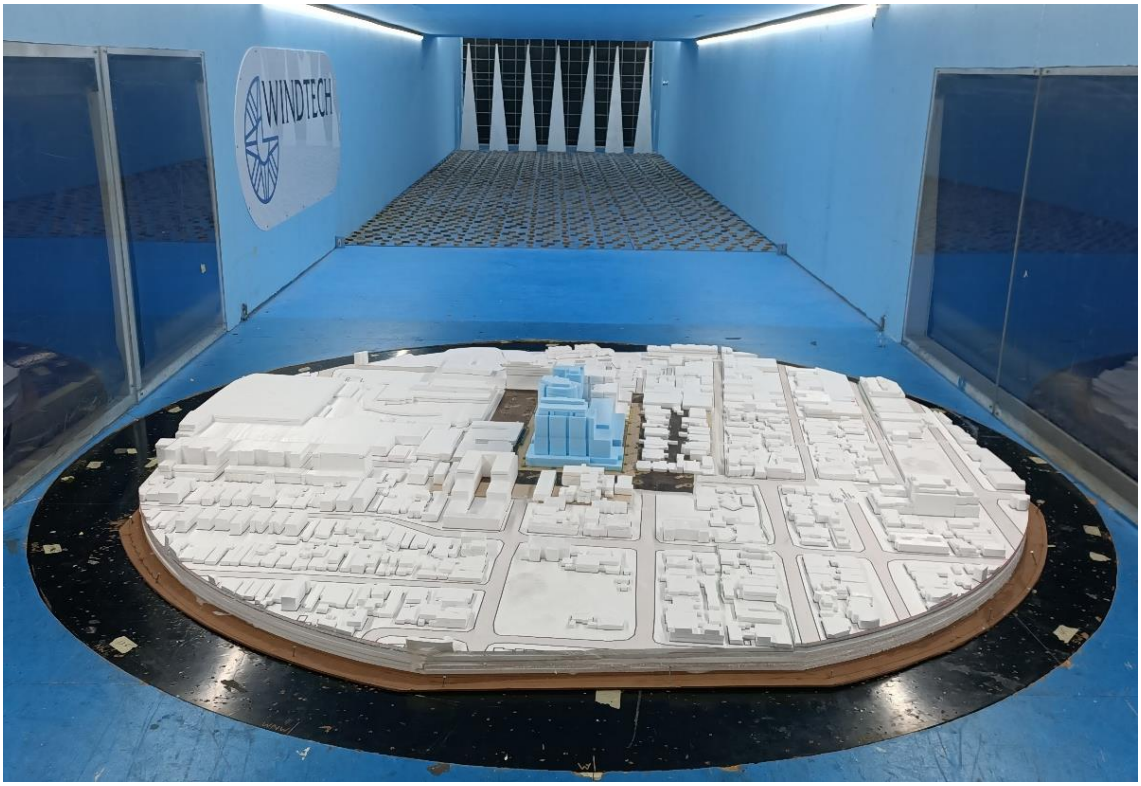


Figure 1e: Photograph of the Wind Tunnel Model (Proposed Site Conditions, view from the west)

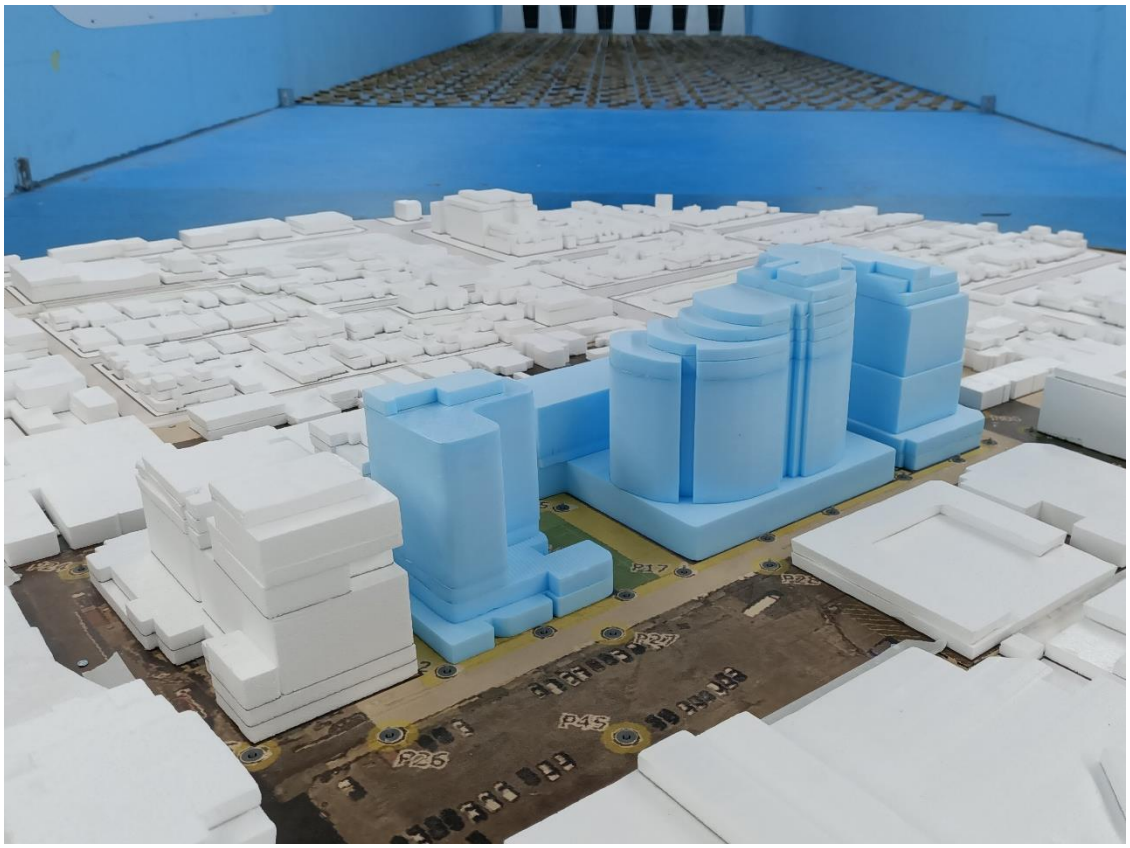


Figure 1f: Photograph of the Wind Tunnel Model (Proposed Site Conditions, close-up view from the north-east)

Figure 1g: Photograph of the Wind Tunnel Model (Existing Site Conditions, close-up view from the north-east)

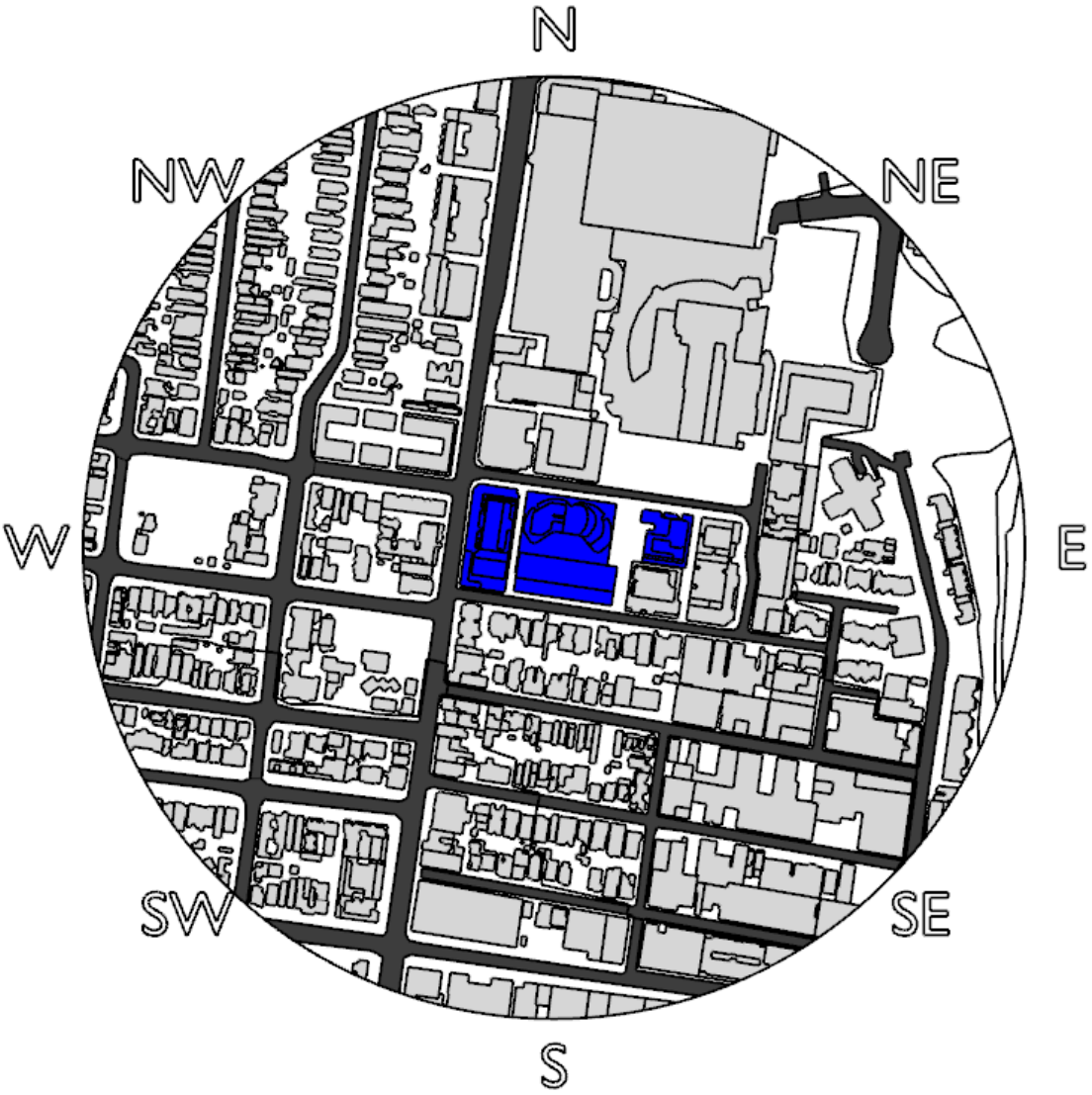


Figure 2a: Proximity Model Plan (Proposed Site Conditions)

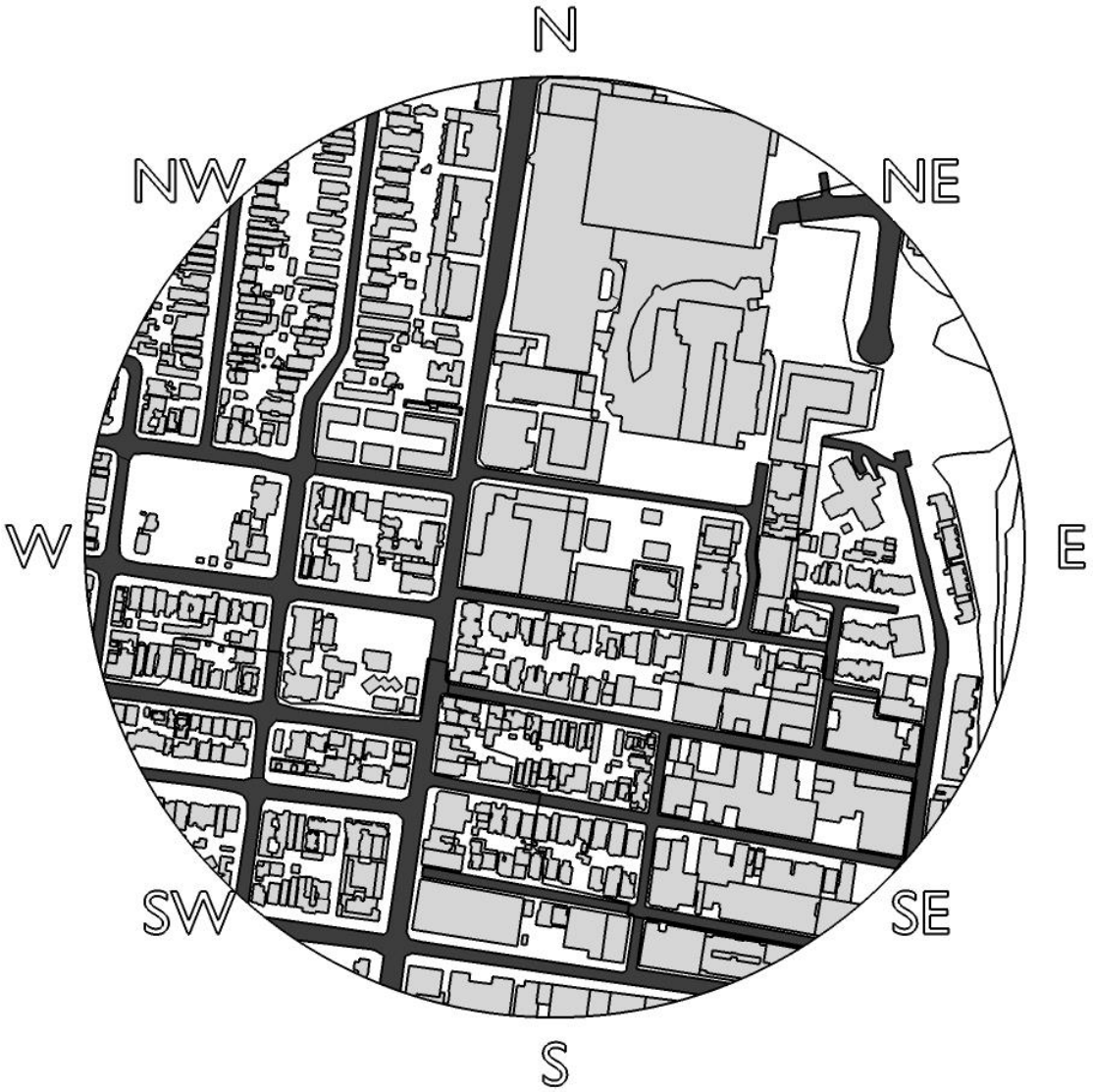


Figure 2b: Proximity Model Plan (Existing Site Conditions)

3 BOUNDARY LAYER WIND PROFILES AT THE SITE

The roughness of the surface of the earth has the effect of slowing down the wind near the ground. This effect is observed up to the boundary layer height, which can range between 500m to 3km above the earth's surface depending on the roughness of the surface (ie: oceans, open farmland, etc). Within this range the prevailing wind forms a boundary layer wind profile.

Various wind codes and standards and other publications classify various types of boundary layer wind flows depending on the surface roughness z_0. Descriptions of typical boundary layer wind profiles, based on D.M. Deaves and R.I. Harris (1978), are summarised as follows:

- Flat terrain (0.002m < z_0 < 0.003m). Examples include inland water bodies such as lakes, dams, rivers, etc, and the open ocean.
- Semi-open terrain (0.006m < z_0 < 0.01m). Examples include flat deserts and plains.
- Open terrain (0.02m < z_0 < 0.03m). Examples include grassy fields, semi-flat plains, and open farmland (without buildings or trees).
- Semi-suburban/semi-forest terrain (0.06m < z_0 < 0.1m). Examples include farmland with scattered trees and buildings and very low-density suburban areas.
- Suburban/forest terrain (0.2m < z_0 < 0.3m). Examples include suburban areas of towns and areas with dense vegetation such as forests, bushland, etc.
- Semi-urban terrain (0.6m < z_0 < 1.0m). Examples include centres of small cities, industrial parks, etc.
- Urban terrain (2.0m < z_0 < 3.0m). Examples include centres of large cities with many high-rise towers, and also areas with many closely-spaced mid-rise buildings.

The boundary layer wind profile does not change instantly due to changes in the terrain roughness. It can take many kilometres (at least 100km) of a constant surface roughness for the boundary layer wind profile to achieve a state of equilibrium. Hence an analysis of the effect of changes in the upwind terrain roughness is necessary to determine an accurate boundary layer wind profile at the development site location.

The proximity model accounts for the effect of the near field topographic effects as well as the influence of the local built forms. To account for further afield effects, an assessment of the upwind terrain roughness has been undertaken based on the method given in AS/NZS1170.2:2021, using a fetch ranging from 20 to 60 times the study reference height (as per the recommendation by AS/NZS1170.2:2021). An aerial image showing the surrounding terrain is presented in Figure 3 for a range of 1.8 km from the edge of the proximity model used for the wind tunnel study. The resulting mean and gust terrain and height multipliers at the site location are presented in Table 1, referenced to the study reference height (which is approximately half the height of the subject development since typically we are most interested in the wind effects at the ground plane). Details of the boundary layer wind profiles at the site are combined with the regional wind model (see Section 4) to determine the site wind speeds.

Table 1: Approaching Boundary Layer Wind Profile Analysis Summary (at the study reference height)

Wind Sector (degrees)	Terrain and Height Multiplier			Turbulence Intensity	Equivalent Terrain Category (AS/NZS1170.2:2011 naming convention)
	$k_{tr,T=1hr}$ (hourly)	$k_{tr,T=10min}$ (10min)	$k_{tr,T=3s}$ (3sec)	I_v	
0	0.64	0.68	1.05	0.213	2.8
30	0.64	0.67	1.05	0.216	2.9
60	0.61	0.65	1.03	0.225	3.0
90	0.61	0.65	1.03	0.225	3.0
120	0.61	0.65	1.03	0.225	3.0
150	0.67	0.71	1.07	0.200	2.7
180	0.63	0.66	1.04	0.220	2.9
210	0.59	0.63	1.01	0.238	3.1
240	0.61	0.65	1.03	0.225	3.0
270	0.58	0.62	1.00	0.246	3.2
300	0.59	0.63	1.01	0.242	3.1
330	0.64	0.68	1.05	0.214	2.9

NOTE: These terrain and height multipliers are to be applied to a basic regional wind speed averaged over 3-seconds. Divide these values by 1.10 for a basic wind speed averaged over 0.2-seconds, 0.69 for a basic wind speed averaged over 10-minutes, or 0.66 for a basic wind speed averaged over 1-hour.

For each of the 16 wind directions tested in this study, the approaching boundary layer wind profiles modelled in the wind tunnel closely matched the profiles listed in Table 1. Plots of the boundary layer wind profiles used for the wind tunnel testing are presented in Appendix D of this report.

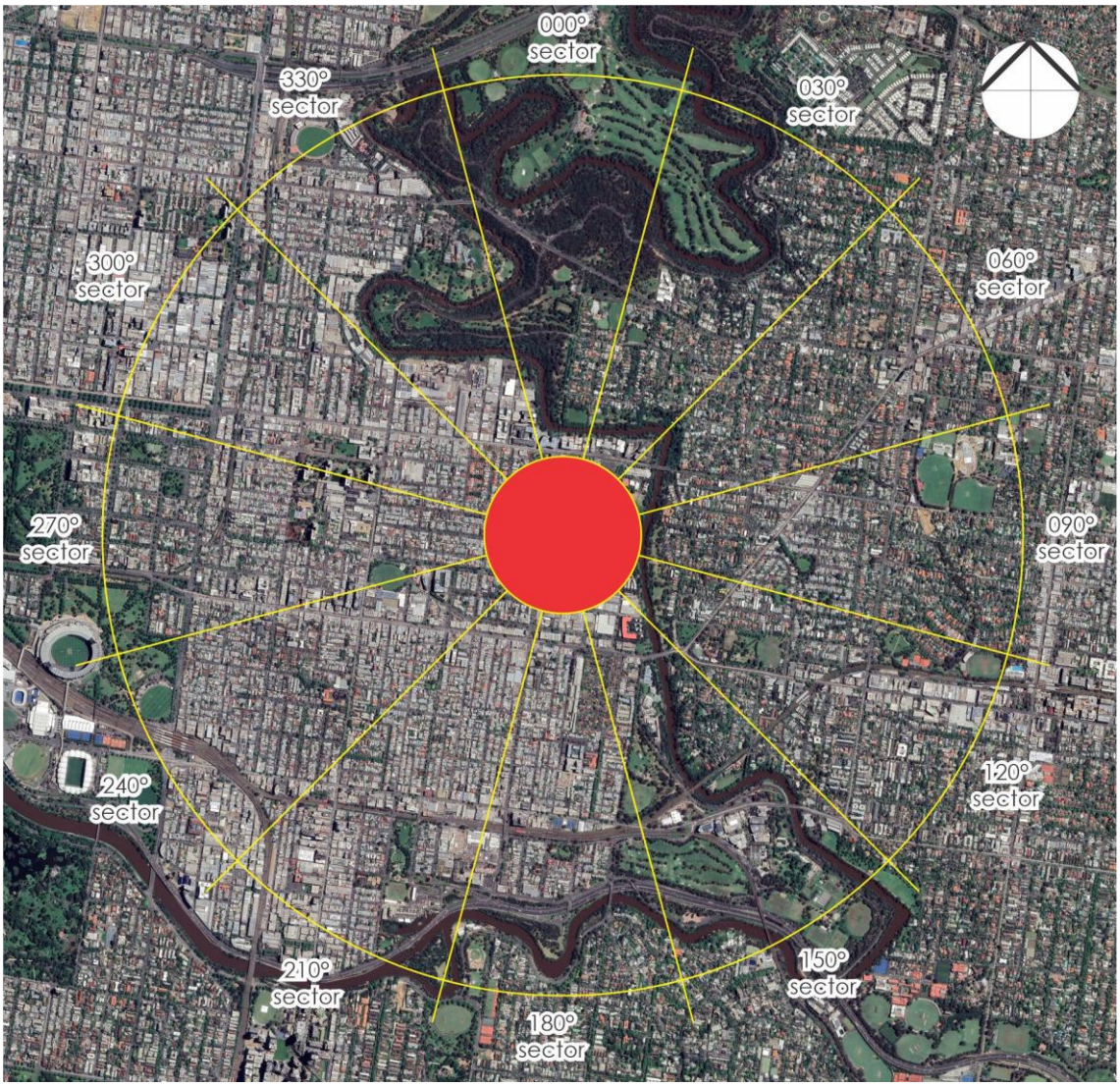


Figure 3: Aerial Image of the Surrounding Terrain (radius of 1.8 km from the edge of the proximity model)

4 REGIONAL WIND MODEL

The regional wind model used in this study was determined from an analysis of measured directional mean wind speeds obtained at the meteorological recording station located at the Melbourne Airport. Data was collected from 1970 to 2009 and corrected so that it represents winds over standard open terrain at a height of 10m above ground for each wind direction. From this analysis, directional probabilities of exceedance and directional wind speeds for the region are determined. The directional wind speeds are summarised in Table 2. The directional wind speeds and corresponding directional frequencies of occurrence are presented in Figure 4.

The northerly winds are by far the most frequent wind for the Melbourne region and the strongest. The southerly winds occur most frequently during the warmer months of the year. The far less frequent westerly winds are usually a cold wind since these occur during the spring and winter months and hence can be a cause for discomfort for outdoor areas. The northerly and southerly winds occur most frequently during the warmer months of the year for the Melbourne region, and hence are usually welcomed within outdoor areas.

The recurrence intervals examined in this study are for exceedances of 5% (per 90 degree sector) of the pedestrian comfort criteria using Gust-Equivalent Mean (GEM) wind speeds, and annual maximum wind speeds (per 22.5 degree sector) for the pedestrian safety criterion. Note that the 5% probability wind speeds presented in Table 2 are only used for the directional plot presented in Figure 4 and are not used for the integration of the probabilities.

Table 2: Regional Directional Wind Speeds (hourly means, at 10m height in standard open terrain) (m/s)

Wind Direction	20% Exceedance	Annual Maximum
N	10.1	15.7
NNE	0.5	11.4
NE	0.5	6.9
ENE	0.5	4.8
E	0.5	5.2
ESE	0.5	6.1
SE	0.5	8.8
SSE	0.5	9.3
S	7.0	11.4
SSW	2.9	10.5
SW	3.1	11.4
WSW	4.1	12.6
W	5.2	12.6
WNW	0.5	10.2
NW	0.5	9.7
NNW	2.3	11.4

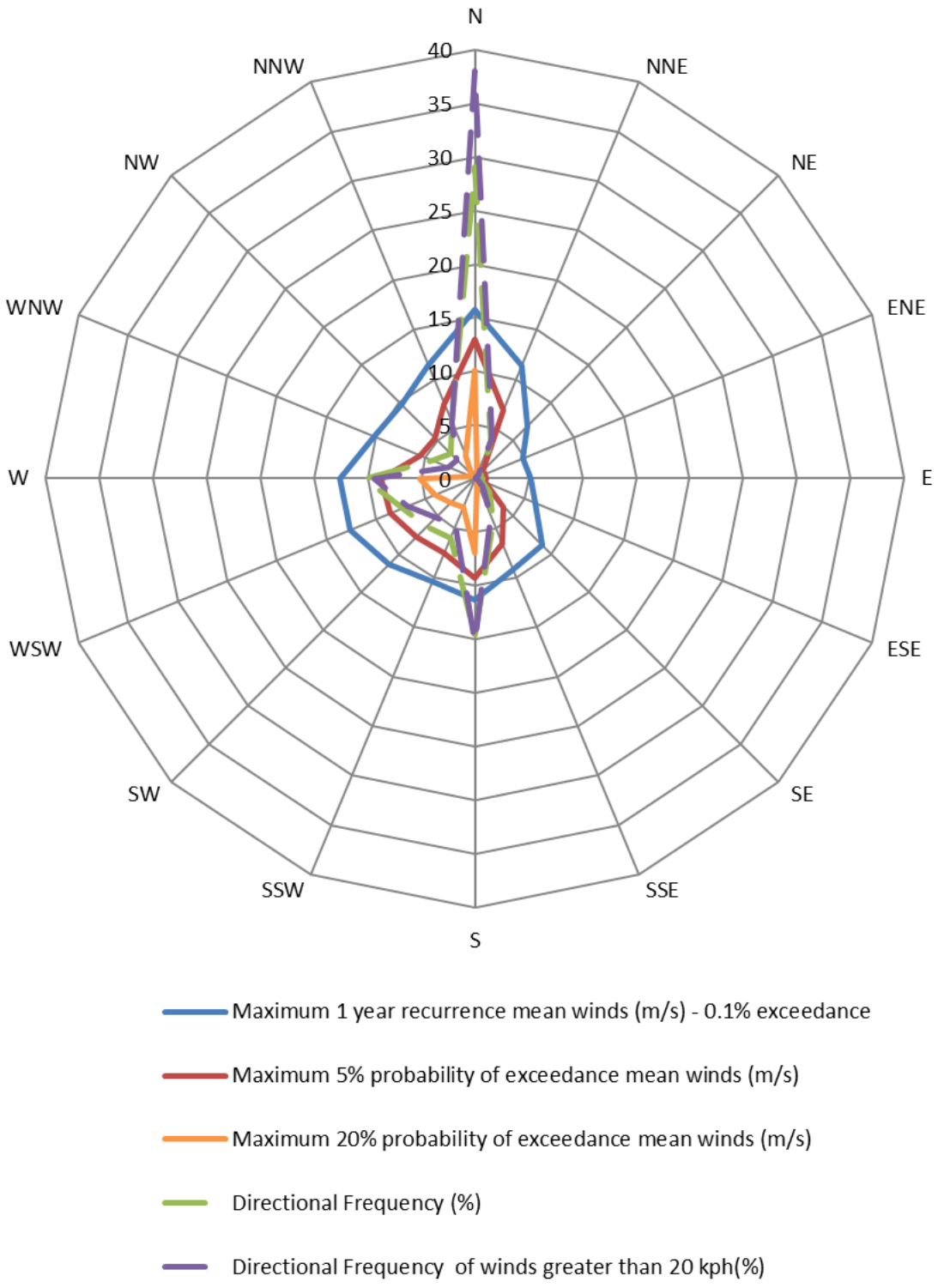


Figure 4: Annual and 5% Exceedance Hourly Mean Wind Speeds, and Frequencies of Occurrence, for the Melbourne Region (at 10m height in standard open terrain)

5 PEDESTRIAN WIND COMFORT AND SAFETY

The acceptability of wind conditions for an area is determined by comparing the measured wind speeds against an appropriate criteria. This section outlines how the measured wind speeds were obtained, the criteria considered for the development, as well as the critical trafficable areas that were assessed and their corresponding criteria designation.

5.1 Measured Wind Speeds

Wind speeds were measured using either Dantec hot-wire probe anemometers or pressure-based wind speed sensors, positioned to monitor wind conditions at critical outdoor trafficable areas of the development. The reference mean free-stream wind speed measured in the wind tunnel, which is at a full-scale height of 200m and measured 3m upstream of the study model.

Measurements were acquired for 16 wind directions at 22.5 degree increments using a sample rate of 1,024Hz. The full methodology of determining the wind speed measurements at the site from either the Dantec Hot-wire probe anemometers or pressure-based wind speed sensors is provided in Appendix B. Based on the results of the analysis of the boundary layer wind profiles at the site (see Section 3), and incorporating the regional wind model (see Section 4), the data sampling length of the wind tunnel test for each wind direction corresponds to a full-scale sample length ranging between 30 minutes and 1 hour. Research by A.W. Rofail and K.C.S. Kwok (1991) has shown that, in addition to the mean and standard deviation of the wind being stable for sample lengths of 15 minutes or more (full-scale), the peak value determined using the upcrossing method is stable for sample lengths of 30 minutes or more.

5.2 Wind Speed Criteria Used for This Study

For this study the measured wind conditions of the selected critical outdoor trafficable areas are compared against two sets of criteria; one for pedestrian safety, and one for pedestrian comfort. The safety criterion is applied to the annual maximum gust winds, and the comfort criteria is applied to Gust Equivalent Mean (GEM) winds. In accordance with ASCE (2003), the GEM wind speed is defined as follows:

$$GEM = max\left(\bar{V}, \frac{\hat{V}}{1.85}\right) \tag{5.1}$$

where:

- $\bar{V}$ is the mean wind speed.
- $\hat{V}$ is the 3-second gust wind speed.

The measured wind conditions for the various critical outdoor trafficable areas around the subject development are compared against the Melbourne Planning Scheme Amendment C270 (2016). This requires both the safety limit criteria and wind comfort criteria to be achieved for the various outdoor public areas. The safety criteria states that the 3-second gust wind speed must not exceed 20m/s for more than 0.1% of the time from any given wind direction.

Furthermore, the criteria for wind comfort must not also exceed more than 20% of the time (probability of exceedance) from all directions combined, measured across all hours of the year. The different comfort are presented in Table 3. These criteria are equivalent to the Davenport (1972) criteria. Research by A.W. Rofail (2007) has shown that the Davenport (1972) criteria, used in conjunction with a GEM wind speed, has proven over time and through field observations to be the most reliable indicator of pedestrian comfort. A more detailed comparison of published criteria has been provided in Appendix A.

The criteria considered in this study are summarised in Tables 3 and 4 for pedestrian comfort and safety, respectively. The results of the wind tunnel study are presented in the form of directional plots attached in Appendix C of this report. For each study point there is a plot of the GEM wind speeds using the comfort criteria, and a plot for the annual maximum gust wind speeds using the safety criterion.

Table 3: Comfort Criteria (from Melbourne Planning Scheme Amendment C270, 2016)

Classification	Description	Maximum 20% Exceedance GEM Wind Speed (m/s)
Sitting	Long duration stationary activities such as in outdoor restaurants and theatres, etc.	5.0
Standing	Short duration stationary activities (generally less than 1 hour), including window shopping, waiting areas, etc.	4.0
Walking	For pedestrian thoroughfares, private swimming pools, most communal areas, private balconies and terraces, etc.	3.0

Table 4: Safety Criterion (from W.H. Melbourne, 1978)

Classification	Description	Annual Maximum Gust Wind Speed (m/s)
Safety	Safety criterion applies to all trafficable areas.	20

5.3 Layout of Study Points

For this study a total of 45 study points along the pedestrian footpaths and other trafficable areas within and around the masterplan development were selected for analysis in the wind tunnel. The locations of the various study points tested for this study, as well as the target wind speed criteria for the various outdoor trafficable areas of the development, are presented in Figures 5 in the form of marked-up plans. It should be noted that only the most critical outdoor locations of the development have been selected for analysis.

Figure 5: Study Point Locations and Target Wind Speed Criteria – Ground Floor Plan

6 RESULTS AND DISCUSSION

The results of the wind tunnel study are presented in the form of directional plots in Appendix C for all study points locations, summarised in Tables 5 and 6, and shown on marked-up plans in Figure 6. The wind speed criteria that the wind conditions should achieve are also listed in Tables 5 and 6 for each study point location, as well as in Figures 5.

The results of the study indicate that wind conditions for many trafficable outdoor locations within and around the development will be suitable for their intended uses. Some areas will experience strong winds which will exceed the safety criteria or the existing site conditions. Additional wind tunnel testing was conducted with the inclusion of the treatment scheme detailed below and indicated in Figures 7. The results of the additional testing indicated the treatment scheme was effective in wind mitigation and the outdoor trafficable areas within and around the development site will meet the safety limit criterion, or are equivalent/better than the existing site conditions. Of the various study points tested, the results show that the wind conditions at locations 25, 26 and 43 already exceed the safety limit. The results of the study indicate the proposed development does not exacerbate the existing strong wind conditions at these three study points which are predominantly exposed to direct wind effects travelling over the adjacent open carpark from the prevailing northerly direction. It should be noted the strong wind conditions at these locations are likely be improved or resolved with the inclusion of the Victoria Gardens development across Doonside Street to the north.

It should be noted that the treatment scheme is indicative for the current design of the development and verifies that wind conditions within the critical outdoor trafficable locations within and around can achieve the safety limit or are equivalent/better than to the existing site conditions. As the design is developed for the planning permit application, further modelling will be undertaken to optimise the scale and extent of the required treatments to suit the detailed design.

The tested treatments that have been demonstrated to meet the safety limit or existing site conditions are detailed as follows:

Doonside Park:

- Inclusion of 1-1.5m high raised garden beds along the public open space.
- Strategic inclusion of impermeable screens atop of the raised garden beds, with an overall height of 2.5m from the local ground level.
- Inclusion of a 2.5m high porous screen along the perimeter edge of the proposed paving at the centre of the public open space. The porosity of the screen is to be a maximum of 30%.
- The proposed bench adjacent to the heritage building is to have a 1.5m high impermeable backrest.

Building A:

- Inclusion of impermeable awnings along the northern and western façade of the podium.
- Inclusion of a Level 1 porous canopy along the eastern façade of the podium (between Buildings A and B) with a maximum porosity of 30%.

- Inclusion of fixed openings within the existing ground level windows/door systems at the north-western corner.
- An extension of the proposed north-western lobby entrance further along the southern boundary.
- Inclusion of 1.5m high impermeable balustrades on the Level 2 podium. The impermeable balustrade is to be offset 1.5m away from the podium edge along the northern and western boundaries.
- Inclusion of a north-western corner 4m x 4m wide balcony on all levels of the tower. A full-height porous screen is also to be included along the western perimeter edge of the balconies with a maximum porosity of 30%.

Building B:

- Inclusion of Level 2 impermeable awnings along the northern façade of the podium.
- Inclusion of a Level 2 porous canopy along the eastern façade of the podium with a maximum porosity of 30%.

Building C:

- Inclusion of 3m high impermeable screens along the north-western perimeter edge of the Level 2 podium rooftop.
- Inclusion of a porous canopy atop of the abovementioned 3m high impermeable screen. The porosity of the canopy is to be a maximum of 30%.
- Inclusion of 3m high porous screen along most of the eastern edge of the Level 2 podium rooftop.
- Inclusion of a north-eastern corner 3m x 3m wide balcony on all levels of the tower. A full-height porous screen is also to be included along the eastern perimeter edge of the balconies with a maximum porosity of 30%.

It should be noted that many of these issues are due to funnelling, downwash and corner acceleration effects of the northerly winds and will likely be significantly improved or resolved with the inclusion of the Victoria Gardens development across Doonside Street to the north.

A further investigation was undertaken with the wind speed measurements for the critical outdoor trafficable locations compared against the applicable criteria for pedestrian comfort. The results of the study indicate that wind conditions for many trafficable outdoor locations within and around the development will be suitable for their intended uses. Some areas will experience strong winds which will exceed the relevant criteria for wind comfort. Suggested in-principle treatments are described in Appendix E.

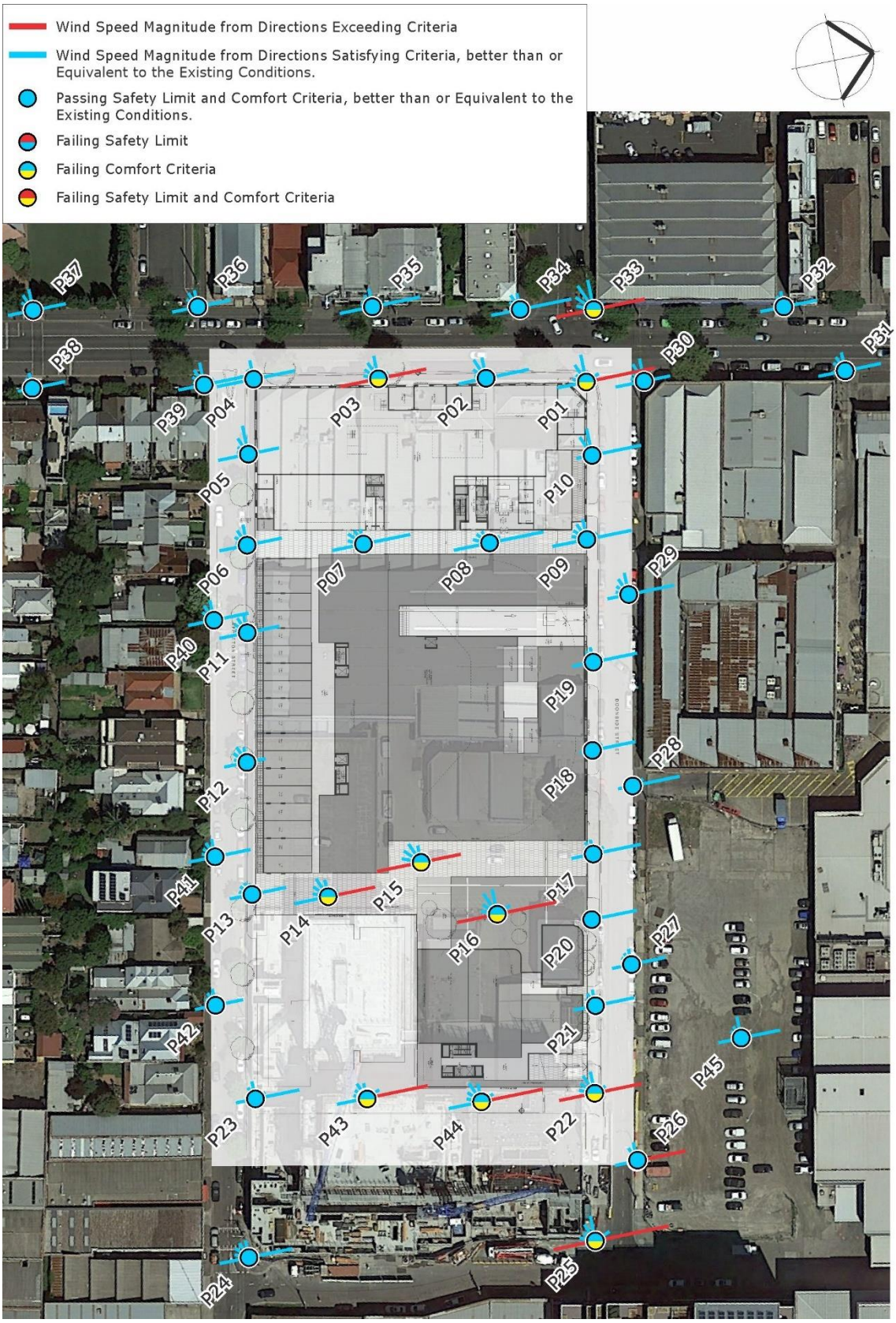


Figure 6: Wind Tunnel Results – Ground Floor Plan
(results shown with the inclusion of the treatment scheme)

Table 5: Wind Tunnel Results Summary – Annual Gust vs Safety Limit

Study Point	Annual Gust			Final Result	Description of Treatment
	Criterion (m/s)	Results (m/s)	Grade		
P01	20	20	Pass	Pass	Refer to Figures 7a to 7e.
Existing		19	Pass		
P02	20	18	Pass	Pass	Refer to Figures 7a to 7e.
Existing		14	Pass		
P03	20	20	Pass	Pass	Refer to Figures 7a to 7e.
Existing		14	Pass		
P04	20	17	Pass	Pass	Refer to Figures 7a to 7e.
Existing		14	Pass		
P05	20	18	Pass	Pass	
Existing		15	Pass		
P06	20	20	Pass	Pass	
Existing		13	Pass		
P07	20	16	Pass	Pass	Refer to Figures 7a to 7e.
P08	20	20	Pass		Refer to Figures 7a to 7e.
P09	20	17	Pass	Pass	Refer to Figures 7a to 7e.
Existing		15	Pass		
P10	20	20	Pass	Pass	Refer to Figures 7a to 7e.
Existing		18	Pass		
P11	20	14	Pass	Pass	
Existing		13	Pass		
P12	20	15	Pass	Pass	
Existing		17	Pass		
P13	20	20	Pass	Pass	
Existing		15	Pass		
P14	20	20	Pass	Pass	Refer to Figures 7a to 7e.
P15	20	17	Pass		Refer to Figures 7a to 7e.
Existing		20	Pass	Pass	
P16	20	20	Pass		Refer to Figures 7a to 7e.
Existing		20	Pass	Pass	
P17	20	20	Pass		Refer to Figures 7a to 7e.
Existing		19	Pass	Pass	
P18	20	20	Pass		
Existing		16	Pass	Pass	
P19	20	19	Pass		
Existing		18	Pass	Pass	
P20	20	19	Pass		Refer to Figures 7a to 7e.
Existing		20	Pass	Pass	
P21	20	17	Pass		

Study Point	Annual Gust			Final Result	Description of Treatment
	Criterion (m/s)	Results (m/s)	Grade		
Existing		19	Pass	Pass	
P22	20	19	Pass		Refer to Figures 7a to 7e.
Existing		24	Fail	Pass	
P23	20	20	Pass		
Existing		21	Fail	Pass	
P24	20	18	Pass		
Existing		18	Pass	Pass	
P25	20	26	Fail		Refer to Figures 7a to 7e..
Existing		26	Fail	Pass	
P26	20	21	Fail		Better than or equivalent to Existing Conditions.
Existing		23	Fail	Pass	
P27	20	15	Pass		
Existing		17	Pass	Pass	
P28	20	20	Pass		Refer to Figures 7a to 7e.
Existing		21	Fail	Pass	
P29	20	19	Pass		Refer to Figures 7a to 7e.
Existing		15	Pass	Pass	
P30	20	20	Pass		
Existing		15	Pass	Pass	
P31	20	15	Pass		
Existing		16	Pass	Pass	
P32	20	14	Pass		
Existing		17	Pass	Pass	
P33	20	19	Pass		Refer to Figures 7a to 7e.
Existing		18	Pass	Pass	
P34	20	20	Pass		
Existing		13	Pass	Pass	
P35	20	20	Pass		Refer to Figures 7a to 7e.
Existing		13	Pass	Pass	
P36	20	15	Pass		
Existing		15	Pass	Pass	
P37	20	13	Pass		
Existing		13	Pass	Pass	
P38	20	17	Pass		
Existing		20	Pass	Pass	
P39	20	16	Pass		Refer to Figures 7a to 7e.
Existing		14	Pass	Pass	
P40	20	15	Pass		
Existing		15	Pass	Pass	

Study Point	Annual Gust			Final Result	Description of Treatment
	Criterion (m/s)	Results (m/s)	Grade		
P41	20	16	Pass		
Existing		15	Pass	Pass	
P42	20	12	Pass		
Existing		13	Pass	Pass	
P43	20	23	Fail		Better than or equivalent to Existing Conditions.
Existing		24	Fail	Pass	
P44	20	20	Pass		Refer to Figures 7a to 7e.
Existing		20	Pass	Pass	
P45	20	17	Pass		
Existing		13	Pass	Pass	

Table 6: Wind Tunnel Results Summary – GEM vs Comfort Criteria for 20% exceedance

Study Point	GEM (20% exceedance)			Description of Treatment
	Criterion (m/s)	Results (%)	Grade	
P01	5.0	27%	Fail	Refer to In-principal recommendations in Appendix E
Existing		18%	Pass	
P02	5.0	16%	Pass	
Existing		5%	Pass	
P03	5.0	24%	Fail	Refer to In-principal recommendations in Appendix E
Existing		8%	Pass	
P04	5.0	16%	Pass	
Existing		7%	Pass	
P05	5.0	14%	Pass	
Existing		4%	Pass	
P06	5.0	19%	Pass	
Existing		5%	Pass	
P07	5.0	17%	Pass	
P08	5.0	20%	Pass	
P09	5.0	19%	Pass	
Existing		7%	Pass	
P10	5.0	20%	Pass	
Existing		14%	Pass	
P11	5.0	9%	Pass	
Existing		3%	Pass	
P12	5.0	10%	Pass	
Existing		13%	Pass	

Study Point	GEM (20% exceedance)			Description of Treatment
	Criterion (m/s)	Results (%)	Grade	
P13	5.0	16%	Pass	
Existing		9%	Pass	
P14	5.0	22%	Fail	Refer to In-principal recommendations in Appendix E
P15	5.0	29%	Fail	Refer to In-principal recommendations in Appendix E
Existing		13%	Pass	
P16	4.0	35%	Fail	Refer to In-principal recommendations in Appendix E
Existing		25%	Fail	
P17	5.0	15%	Pass	
Existing		14%	Pass	
P18	5.0	14%	Pass	
Existing		11%	Pass	
P19	5.0	15%	Pass	
Existing		12%	Pass	
P20	5.0	10%	Pass	
Existing		16%	Pass	
P21	5.0	12%	Pass	
Existing		13%	Pass	
P22	5.0	23%	Fail	Refer to In-principal recommendations in Appendix E
Existing		22%	Fail	
P23	5.0	15%	Pass	
Existing		18%	Pass	
P24	5.0	14%	Pass	
Existing		14%	Pass	
P25	5.0	34%	Fail	Refer to In-principal recommendations in Appendix E
Existing		25%	Fail	
P26	5.0	14%	Pass	
Existing		24%	Fail	
P27	5.0	7%	Pass	
Existing		12%	Pass	
P28	5.0	14%	Pass	
Existing		19%	Pass	
P29	5.0	16%	Pass	
Existing		6%	Pass	
P30	5.0	16%	Pass	
Existing		10%	Pass	
P31	5.0	9%	Pass	
Existing		11%	Pass	
P32	5.0	6%	Pass	
Existing		14%	Pass	

Study Point	GEM (20% exceedance)			Description of Treatment
	Criterion (m/s)	Results (%)	Grade	
P33	5.0	31%	Fail	Refer to In-principal recommendations in Appendix E
Existing		15%	Pass	
P34	5.0	19%	Pass	
Existing		5%	Pass	
P35	5.0	16%	Pass	
Existing		5%	Pass	
P36	5.0	8%	Pass	
Existing		6%	Pass	
P37	5.0	5%	Pass	
Existing		4%	Pass	
P38	5.0	12%	Pass	
Existing		22%	Fail	
P39	5.0	14%	Pass	
Existing		4%	Pass	
P40	5.0	7%	Pass	
Existing		7%	Pass	
P41	5.0	12%	Pass	
Existing		8%	Pass	
P42	5.0	3%	Pass	
Existing		3%	Pass	
P43	5.0	21%	Pass	Better than or equivalent to Existing Conditions.
Existing		31%	Fail	
P44	5.0	24%	Fail	Refer to In-principal recommendations in Appendix E
Existing		16%	Pass	
P45	5.0	12%	Pass	
Existing		5%	Pass	

Note that, for any study points listed in Tables 5 and 6 with two rows of results data, the second row is for the existing site conditions. The test results shown in Tables 5 and 6 are without any treatments applied. If treatment is required, the treatment is described in Tables 5 and 6.

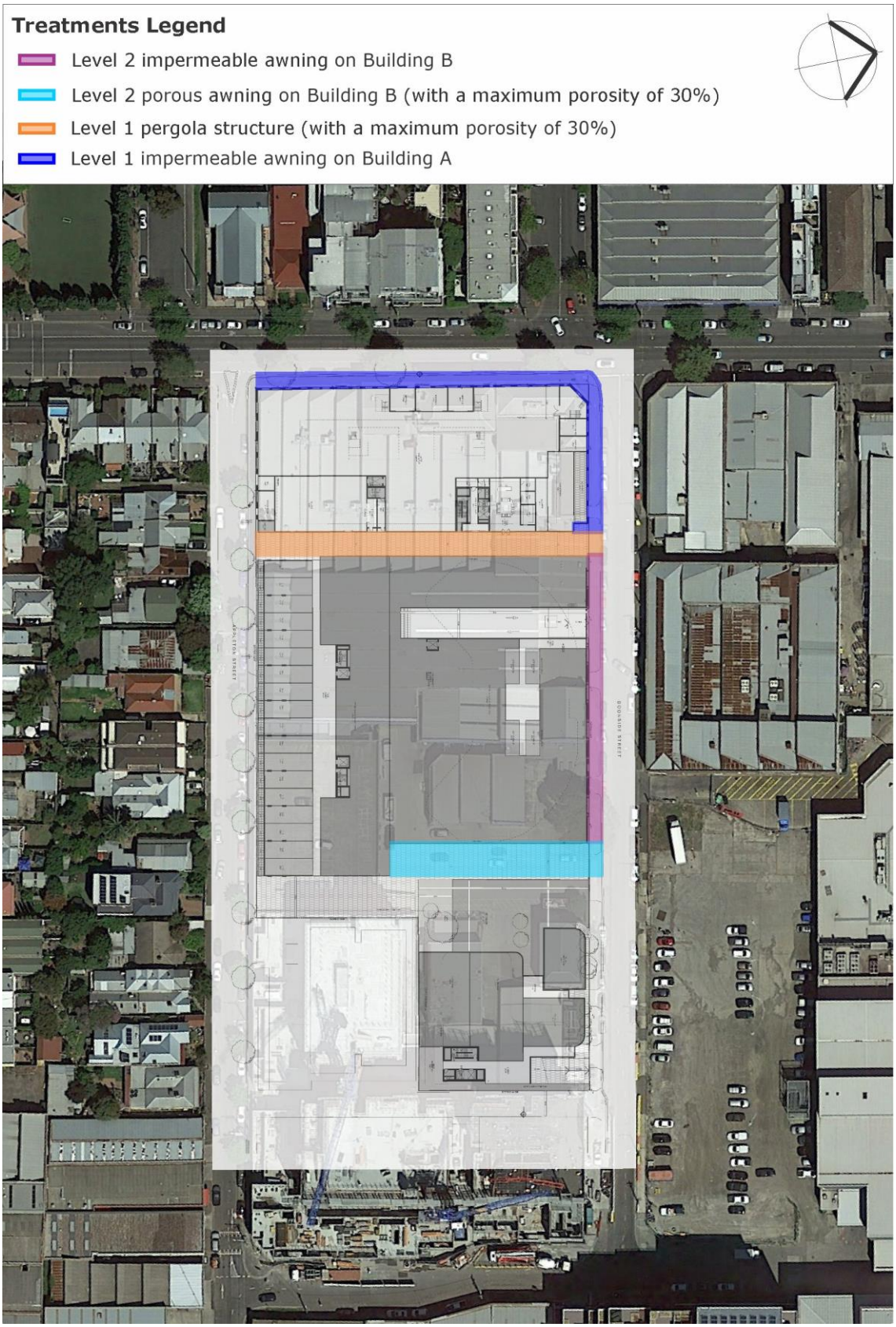


Figure 7a: Treatment Scheme – Level 1 and Level 2 Awnings on Buildings A and B

Figure 7b: Treatment Scheme – Doonside Park Communal Open Space

Figure 7c: Treatment Scheme – Building A – Proposed Lobby

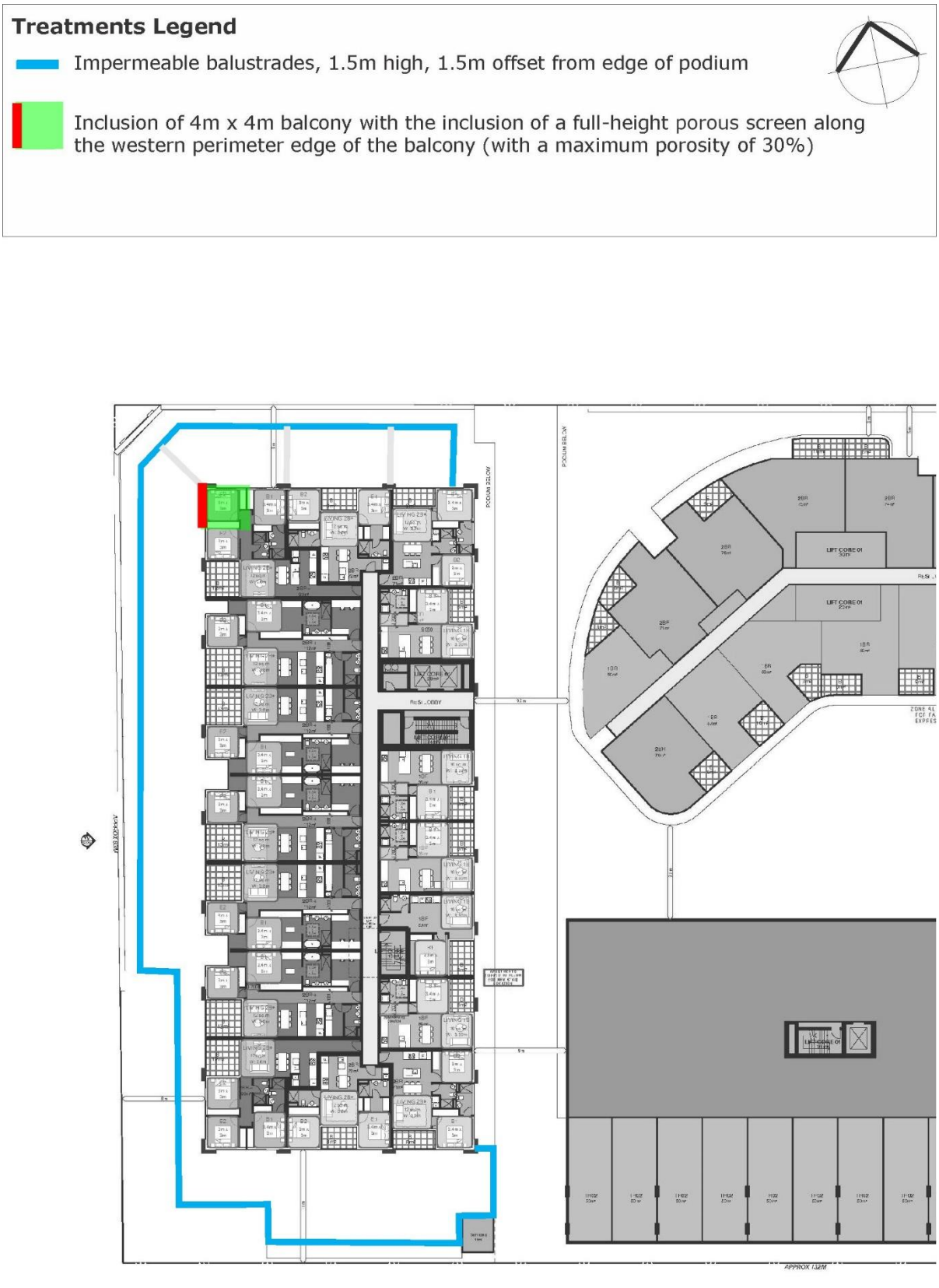


Figure 7d: Treatment Scheme – Building A – Level 2 Podium and Tower Balconies

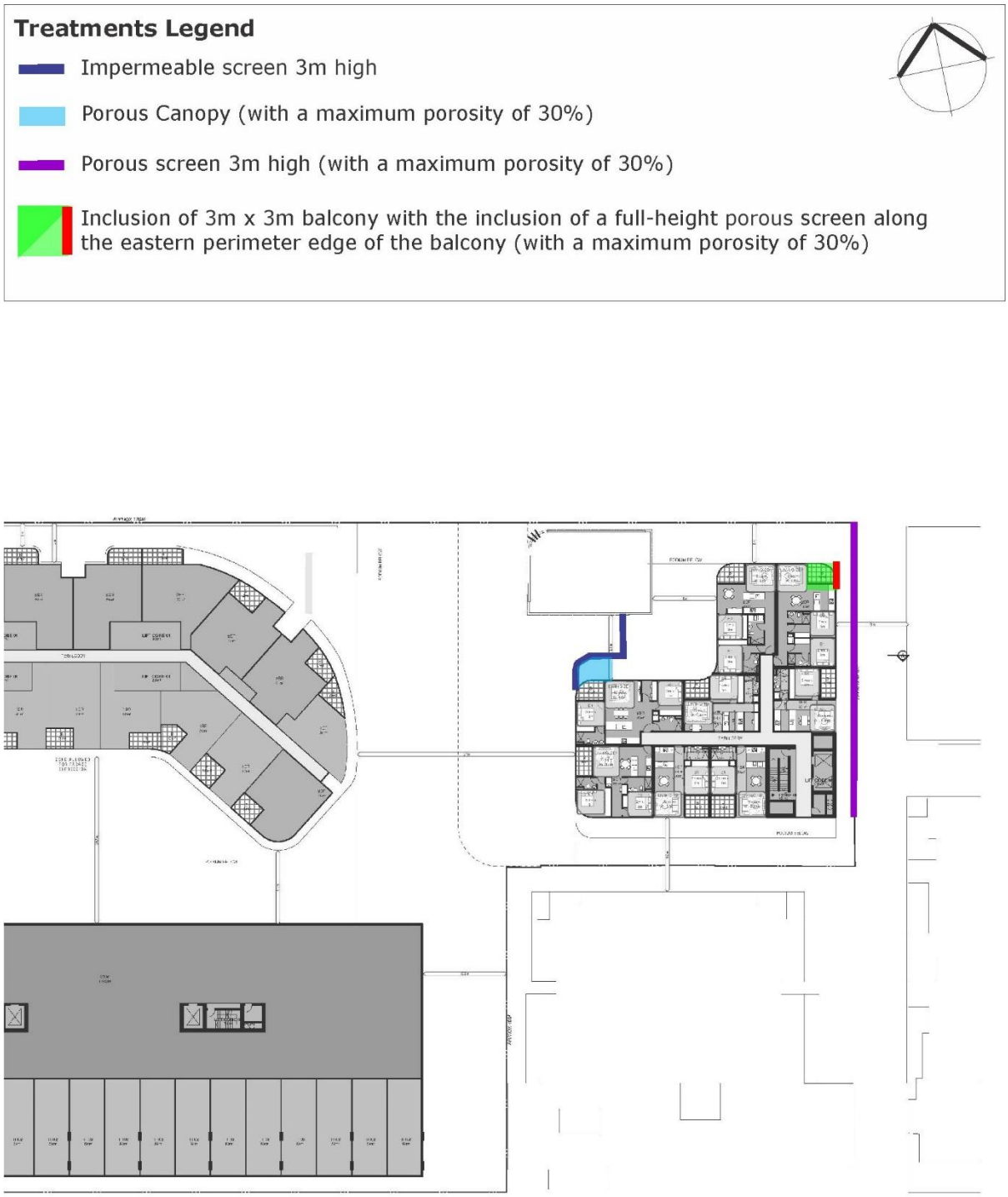


Figure 7e: Treatment Scheme – Building C – Level 2 Podium and Tower Balconies

7 REFERENCES

American Society of Civil Engineers (ASCE), 2003, "Outdoor Human Comfort and its Assessment – State of the Art".

American Society of Civil Engineers (ASCE), ASCE-7-16, 2016, "Minimum Design Loads for Buildings and Other Structures".

Australasian Wind Engineering Society, QAM-1, 2019, "Quality Assurance Manual: Wind Engineering Studies of Buildings", edited by Rofail A.W., et al.

Australasian Wind Engineering Society (AWES), 2014, "Guidelines for Pedestrian Wind Effects Criteria".

Council on Tall Buildings and Urban Habitat (CTBUH), 2013, "Wind tunnel testing of high-rise buildings", CTBUH Technical Guides.

Davenport, A.G., 1972, "An approach to human comfort criteria for environmental conditions". Colloquium on Building Climatology, Stockholm.

Deaves, D.M. and Harris, R.I., 1978, "A mathematical model of the structure of strong winds." Construction Industry and Research Association (U.K), Report 76.

Engineering Science Data Unit, 1982, London, ESDU82026, "Strong Winds in the Atmospheric Boundary Layer, Part 1: Hourly Mean Wind Speeds", with Amendments A to E (issued in 2002).

Melbourne, W.H., 1978, "Criteria for Environmental Wind Conditions". Journal of Wind Engineering and Industrial Aerodynamics, vol. 3, pp241-249.

Rofail, A.W., and Kwok, K.C.S., 1991, "A Reliability Study of Wind Tunnel Results of Cladding Pressures". Proceedings of the 8th International Conference on Wind Engineering, Canada.

Rofail, A.W., 2007, "Comparison of Wind Environment Criteria against Field Observations". 12th International Conference of Wind Engineering, Cairns, Australia.

Standards Australia and Standards New Zealand, AS/NZS 1170.2, 2011, "SAA Wind Loading Standard, Part 2: Wind Actions".

APPENDIX A PUBLISHED ENVIRONMENTAL CRITERIA

A.1 Wind Effects on People

The acceptability of wind in an area is dependent upon the use of the area. For example, people walking or window-shopping will tolerate higher wind speeds than those seated at an outdoor restaurant. Quantifying wind comfort has been the subject of much research and many researchers, such as A.G. Davenport, T.V. Lawson, W.H. Melbourne, and A.D. Penwarden, have published criteria for pedestrian comfort for pedestrians in outdoor spaces for various types of activities. This section discusses and compares the various published criteria.

A.2 A.D. Penwarden (1973) Criteria for Mean Wind Speeds

A.D. Penwarden (1973) developed a modified version of the Beaufort scale which describes the effects of various wind intensities on people. Table A.1 presents the modified Beaufort scale. Note that the effects listed in this table refers to wind conditions occurring frequently over the averaging time (a probability of occurrence exceeding 5%). Higher ranges of wind speeds can be tolerated for rarer events.

Table A.1: Summary of Wind Effects on People (A.D. Penwarden, 1973)

Type of Winds	Beaufort Number	Hourly Mean Wind Speed (m/s)	Effects
Calm	0	0 - 0.3	
Calm, light air	1	0.3 - 1.6	No noticeable wind
Light breeze	2	1.6 - 3.4	Wind felt on face
Gentle breeze	3	3.4 - 5.5	Hair is disturbed, clothing flaps, newspapers difficult to read
Moderate breeze	4	5.5 – 8.0	Raises dust, dry soil and loose paper, hair disarranged
Fresh breeze	5	8.0 – 10.8	Force of wind felt on body, danger of stumbling
Strong breeze	6	10.8 – 13.9	Umbrellas used with difficulty, hair blown straight, difficult to walk steadily, wind noise on ears unpleasant
Near gale	7	13.9 – 17.2	Inconvenience felt when walking
Gale	8	17.2 - 20.8	Generally impedes progress, difficulty balancing in gusts
Strong gale	9	20.8 – 24.5	People blown over

A.3 A.G. Davenport (1972) Criteria for Mean Wind Speeds

A.G. Davenport (1972) also determined a set of criteria in terms of the Beaufort scale and for various return periods. Table A.2 presents a summary of the criteria based on a probability of exceedance of 5%.

Table A.2: Criteria by A.G. Davenport (1972)

Classification	Activities	5% exceedance Mean Wind Speed (m/s)
Walking Fast	Acceptable for walking, main public accessways.	7.5 - 10.0
Strolling, Skating	Slow walking, etc.	5.5 - 7.5
Short Exposure Activities	Generally acceptable for walking & short duration stationary activities such as window-shopping, standing or sitting in plazas.	3.5 - 5.5
Long Exposure Activities	Generally acceptable for long duration stationary activities such as in outdoor restaurants & theatres and in parks.	0 - 3.5

A.4 T.V. Lawson (1975) Criteria for Mean Wind Speeds

In 1973, T.V. Lawson, while referring to the Beaufort wind speeds of A.D. Penwarden (1973) (as listed in Table A.1), quoted that a Beaufort 4 wind speed would be acceptable if it is not exceeded for more than 4% of the time, and that a Beaufort 6 wind speed would be unacceptable if it is exceeded more than 2% of the time. Later, in 1975, T.V. Lawson presented a set of criteria very similar to those presented in A.G. Davenport (1972) (as listed in Table A.2). These criteria are presented in Table A.3 and Table A.4 for safety and comfort respectively.

Table A.3: Safety Criteria by T.V. Lawson (1975)

Classification	Activities	Annual Mean Wind Speed (m/s)
Safety (all weather areas)	Accessible by the general public.	0 – 15
Safety (fair weather areas)	Private areas, balconies/terraces, etc.	0 – 20

Table A.4: Comfort Criteria by T.V. Lawson (1975)

Classification	Activities	5% exceedance Mean Wind Speed (m/s)
Business Walking	Objective Walking from A to B.	8 - 10
Pedestrian Walking	Slow walking, etc.	6 - 8
Short Exposure Activities	Pedestrian standing or sitting for short times.	4 – 6
Long Exposure Activities	Pedestrian sitting for a long duration.	0 - 4

A.5 W.H. Melbourne (1978) Criteria for Gust Wind Speeds

W.H. Melbourne (1978) introduced a set of criteria for the assessment of environmental wind conditions that were developed for a temperature range of 10°C to 30°C and for people suitably dressed for outdoor conditions. These criteria are presented in Table A.5, and are based on maximum gust wind speeds with a probability of exceedance of once per year.

Table A.5: Criteria by W.H. Melbourne (1978)

Classification	Activities	Annual Gust Wind Speed (m/s)
Limit for Safety	Completely unacceptable: people likely to get blown over.	23
Marginal	Unacceptable as main public accessways.	16 - 23
Comfortable Walking	Acceptable for walking, main public accessways	13 - 16
Short Exposure Activities	Generally acceptable for walking & short duration stationary activities such as window-shopping, standing or sitting in plazas.	10 - 13
Long Exposure Activities	Generally acceptable for long duration stationary activities such as in outdoor restaurants & theatres and in parks.	0 - 10

A.6 Comparison of the Published Wind Speed Criteria

W.H. Melbourne (1978) presented a comparison of the criteria of various researchers on a probabilistic basis. Figure A.1 presents the results of this comparison, and indicates that the criteria of W.H. Melbourne (1978) are comparatively quite conservative. This conclusion was also observed by A.W. Rofail (2007) when undertaking on-site remedial studies. The results of A.W. Rofail (2007) concluded that the criteria by W.H. Melbourne (1978) generally overstates the wind effects in a typical urban setting due to the assumption of a fixed 15% turbulence intensity for all areas. It was observed in A.W. Rofail (2007) that the 15% turbulence intensity assumption is not real and that the turbulence intensities at 1.5m above ground is at least 20% and in a suburban or urban setting is generally in the range of 30% to 60%.

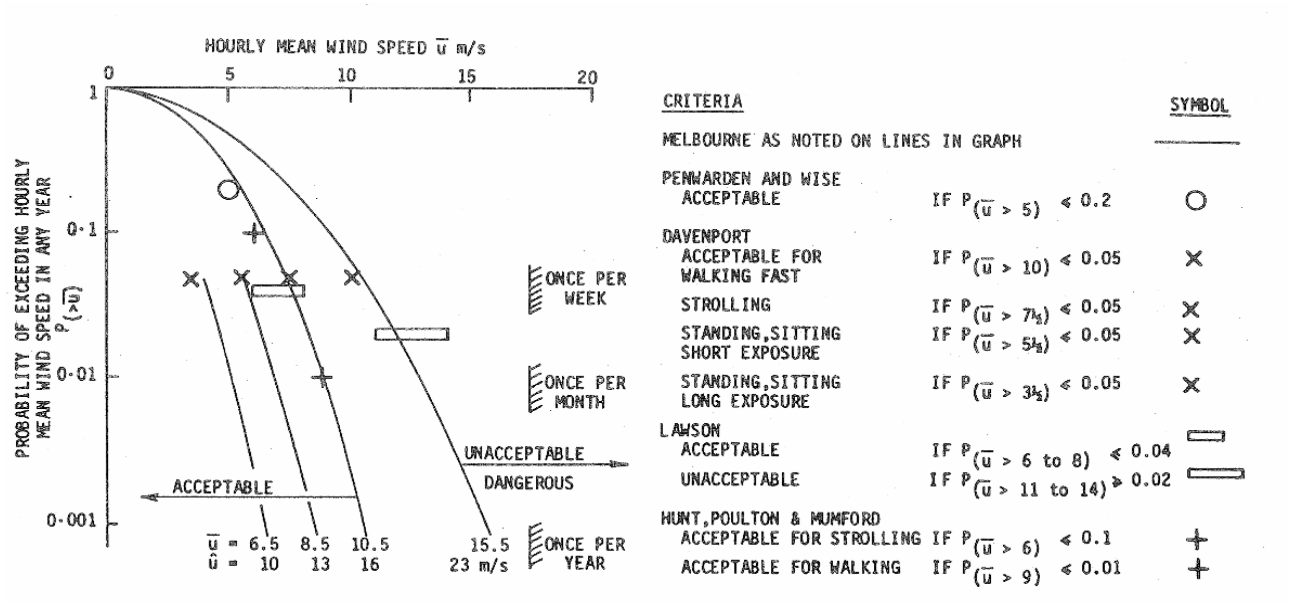


Figure A.1: Comparison of Various Mean and Gust Wind Environment Criteria, assuming 15% turbulence and a Gust Factor of 1.5 (W.H. Melbourne, 1978)

A.7 References relating to Pedestrian Comfort Criteria

Davenport, A.G., 1972, "An approach to human comfort criteria for environmental conditions". Colloquium on Building Climatology, Stockholm.

Davenport, A.G., 1977, "The prediction of risk under wind loading", 2nd International Conference on Structural Safety and Reliability, Munich, Germany, pp511-538.

Lawson, T.V., 1973, "The wind environment of buildings: a logical approach to the establishment of criteria". Bristol University, Department of Aeronautical Engineering.

Lawson, T.V., 1975, "The determination of the wind environment of a building complex before construction". Bristol University, Department of Aeronautical Engineering.

Melbourne, W.H., 1978, "Criteria for Environmental Wind Conditions". Journal of Wind Engineering and Industrial Aerodynamics, vol. 3, pp241-249.

Penwarden, A.D. (1973). "Acceptable Wind Speeds in Towns", Building Science, vol. 8: pp259–267.

Penwarden, A.D., Wise A.F.E., 1975, "Wind Environment Around Buildings". Building Research Establishment Report, London.

Rofail, A.W., 2007, "Comparison of Wind Environment Criteria against Field Observations". 12th International Conference of Wind Engineering, Cairns, Australia.

APPENDIX B DATA ACQUISITION

The wind tunnel testing procedures utilised for this study were based on the guidelines set out in the Australasian Wind Engineering Society Quality Assurance Manual (AWES-QAM-1-2019), ASCE 7-16 (Chapter C31), and CTBUH (2013). The wind speed measurements for the wind tunnel study were determined as coefficients using data acquired by either Dantec hot-wire probe anemometers or pressure-based wind speed sensors and converted to full-scale wind speeds using details of the regional wind climate obtained from an analysis of directional wind speed recordings from the local meteorological recording station(s).

B.1 Measurement of the Velocity Coefficients

The study model and proximity model were setup within the wind tunnel which was configured to the appropriate boundary layer profile, and the wind velocity measurements were monitored using either Dantec hot-wire probe anemometers or pressure-based wind speed sensors at selected critical outdoor locations. The wind velocity results presented in this study for each study point are representative of wind at a full-scale height of approximately 1.5m above ground/slab level. In the case of the Dantec hot-wire probe anemometers, the support of the probe is mounted such that the probe wire is vertical as much as possible to ensure that the measured wind speeds are independent of wind direction along the horizontal plane. In addition, care was taken in the alignment of the hot-wire probe wire and in avoiding wall-heating effects.

Wind speed measurements were made in the wind tunnel for 16 wind directions, at 22.5° increments. Data was acquired for each wind direction using a sample rate of 1024Hz. The sample length was determined to produce a full-scale sample time that is sufficient for this type of study. In the case of the pressure-based wind speed sensors, the phase lag between the various channels where data is acquired simultaneously is within 10% of a typical pressure cycle, and the signal is low-pass filtered at 500Hz and then digital filtering is applied over this range to provide an unbiased response from the pressure measurement system (A.W. Rofail, 2004).

The mean, gust and standard deviation velocity coefficients were determined from the data acquired in the wind tunnel. The gust velocity coefficients were also derived for each wind direction from by the following relation:

$$\hat{C}_V = \bar{C}_V + g \cdot \sigma_{C_V} \qquad \text{B.1}$$

where:

$\hat{C}_V$ is the gust velocity coefficient.

$\bar{C}_V$ is the mean velocity coefficient.

g is the peak factor, taken as 3.0 for a 3-sec gust and 3.4 for a 0.5-sec gust.

σ_{C_V} is the standard deviation of the velocity coefficient measurement.

In the case of a Dantec hot-wire probe anemometer, the velocity coefficient is obtained as follows:

$$C_V = \frac{C_{V,study}}{C_{V,200m}} \quad \text{B.2}$$

where:

$C_{V,study}$ is the velocity coefficient measurement obtained from the Dantec hot-wire probe anemometer at the study point location.

$C_{V,200m}$ is the velocity coefficient measurement obtained from the Dantec hot-wire probe anemometer at the free-stream reference location at 200m height upwind of the model in the wind tunnel.

However, in the case of the pressure-based wind speed sensors, these are determined from the measured differential mean, standard deviation and maximum pressure coefficients obtained from the wind speed sensor. For this analysis all calculations are performed on the square root of the differential pressure measurements. The velocity coefficient at the pressure-based wind speed sensor location is then calculated as follows:

$$C_V = \frac{\alpha + \beta\sqrt{\Delta p}}{V_{200m}} \quad \text{B.3}$$

where:

C_V is the velocity coefficient measurement at the study point location.

α is a calibration coefficient for the pressure-based wind speed sensor.

β is a calibration coefficient for the pressure-based wind speed sensor.

Δp is the differential pressure obtained from the pressure-based wind speed sensor at the study point location.

V_{200m} is the wind speed at the free-stream reference location of 200m height (full-scale) in the wind tunnel, which is determined directly in the wind tunnel using a pitot static probe.

B.2 Calculation of the Full-Scale Results

The full-scale results determine if the wind conditions at a study location satisfy the designated criteria of that location. More specifically, the full-scale results need to determine the probability of exceedance of a given wind speed at a study location. To determine the probability of exceedance, the measured velocity coefficients were combined with a statistical model of the local wind climate that relates wind speed to a probability of exceedance. Details of the wind climate model are outlined in Section 4 of the main report.

The statistical model of the wind climate includes the impact of wind directionality as any local variations in wind speed or frequency with wind direction. This is important as the wind directions that produce the highest wind speed events for a region may not coincide with the most wind exposed direction at the site.

The methodology adopted for the derivation of the full-scale results for the maximum gust and the GEM wind speeds are outlined in the following sub-sections.

B.3 Maximum Gust Wind Speeds

The full-scale maximum gust wind speed at each study point location is derived from the velocity coefficient using the following relationship:

$$V_{study} = V_{ref,RH}\left(\frac{k_{200m,tr,T=1hr}}{k_{RH,tr,T=1hr}}\right)C_V \qquad \text{B.4}$$

where:

V_{study} is the full-scale wind speed at the study point location.

$V_{ref,RH}$ is the full-scale reference wind speed at the study reference height. This value is determined by combining the directional wind speed data for the region (detailed in Section 4) and the upwind terrain and height multipliers for the site (detailed in Section 3).

$k_{200m,tr,T=1hr}$ is the hourly mean terrain and height multiplier at the free-stream reference location of 200m height.

$k_{RH,tr,T=1hr}$ is the hourly mean terrain and height multiplier at the study reference height (Section 3).

C_V is the velocity coefficient, obtained from either Equation B.2 (in the case of Dantec hot-wire probe anemometers) or Equation B.3 (in the case of pressure-based wind speed sensors).

The value of $V_{ref,RH}$ varies with each prevailing wind direction. Wind directions where there is a high probability that a strong wind will occur have a higher directional wind speed than other directions. To determine the directional wind speeds, a probability level must be assigned for each wind direction. These probability levels are set following the approach used in AS/NZS1170.2:2011, which assumes that the major contributions to the combined probability of exceedance of a typical load effect comes from only two 45 degree sectors.

B.4 Maximum Gust-Equivalent Mean Wind Speeds

The contribution to the probability of exceedance of a specified wind speed (ie: the desired wind speed for pedestrian comfort, as per the criteria) was calculated for each wind direction. These contributions are then combined over all wind directions to calculate the total probability of exceedance of the specified wind speed. To calculate the probability of exceedance for a specified wind speed a statistical wind climate model was used to describe the relationship between directional wind speeds and the probability of exceedance. A detailed description of the methodology is given by T.V. Lawson (1980).

The criteria used in this study is referenced to a probability of exceedance of 5% of a specified wind speed.

B.5 References relating to Data Acquisition

American Society of Civil Engineers (ASCE), ASCE-7-16, 2016, "Minimum Design Loads for Buildings and Other Structures".

Australasian Wind Engineering Society, QAM-1, 2019, "Quality Assurance Manual: Wind Engineering Studies of Buildings", edited by Rofail A.W., et al.

Council on Tall Buildings and Urban Habitat (CTBUH), 2013, "Wind tunnel testing of high-rise buildings", CTBUH Technical Guides.

Lawson, T.V., 1980, "Wind Effects on Buildings - Volume 1, Design Applications". Applied Science Publishers Ltd, Ripple Road, Barking, Essex, England.

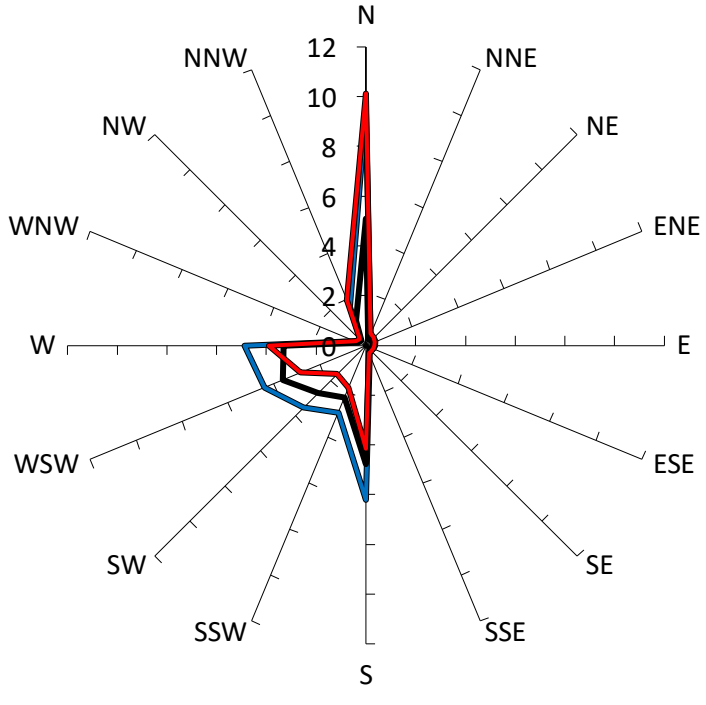
Rofail A.W., Tonin, R., and Hanafi, D., 2004, "Sensitivity of frequency response to type of tubing", Australasian Wind Engineering Workshop, Darwin.

Standards Australia and Standards New Zealand, AS/NZS 1170.2, 2011, "SAA Wind Loading Standard, Part 2: Wind Actions".

APPENDIX C DIRECTIONAL PLOTS OF WIND TUNNEL RESULTS

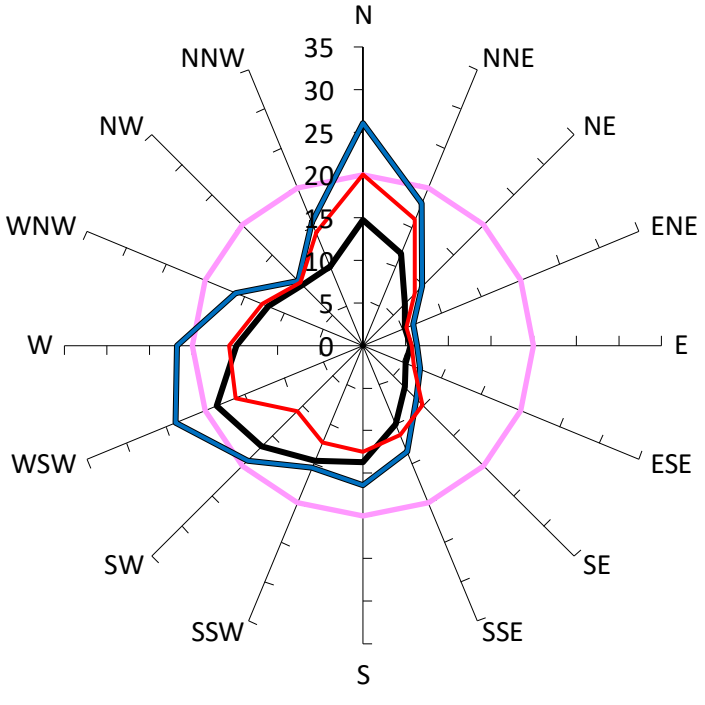
Results for P01

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

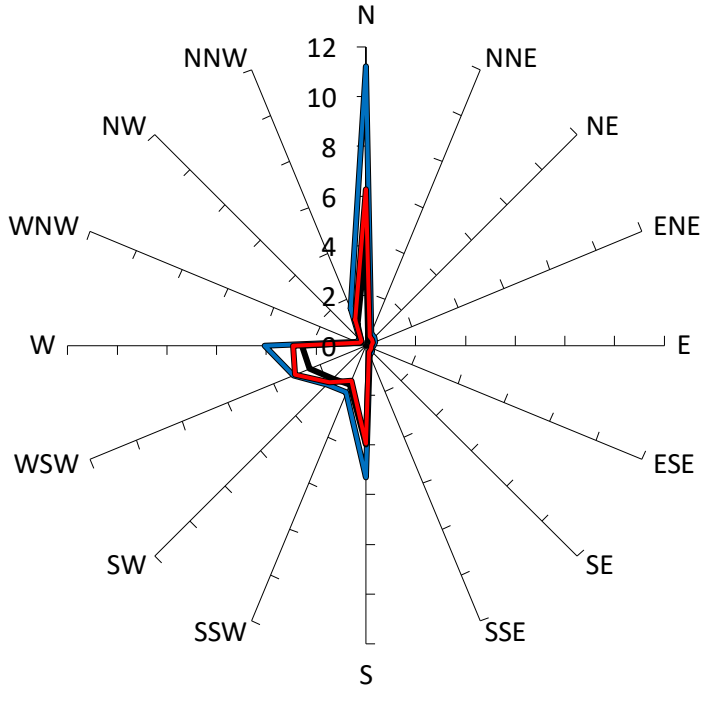


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	39%	26
Existing Site Conditions	18%	19
With the inclusion of the mitigation strategy detailed within the report.	27%	20

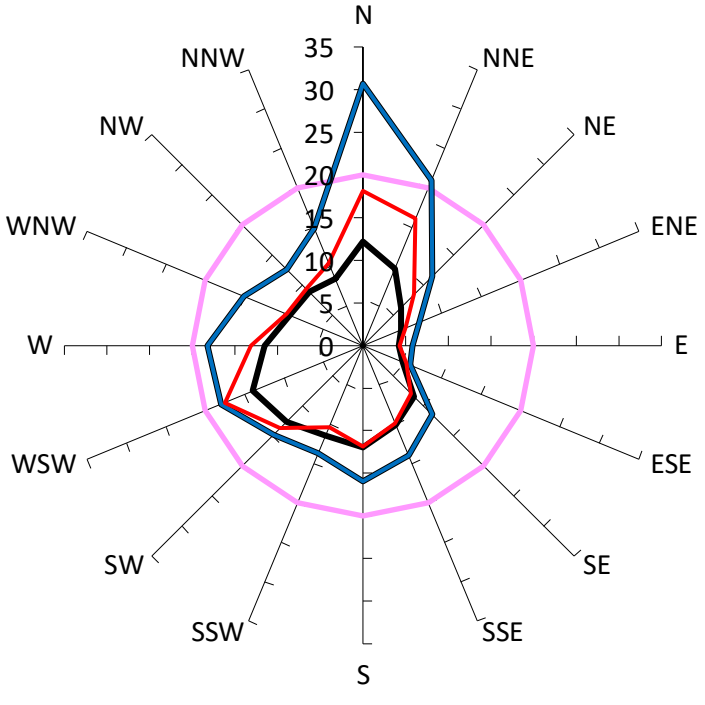
Results for P02

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

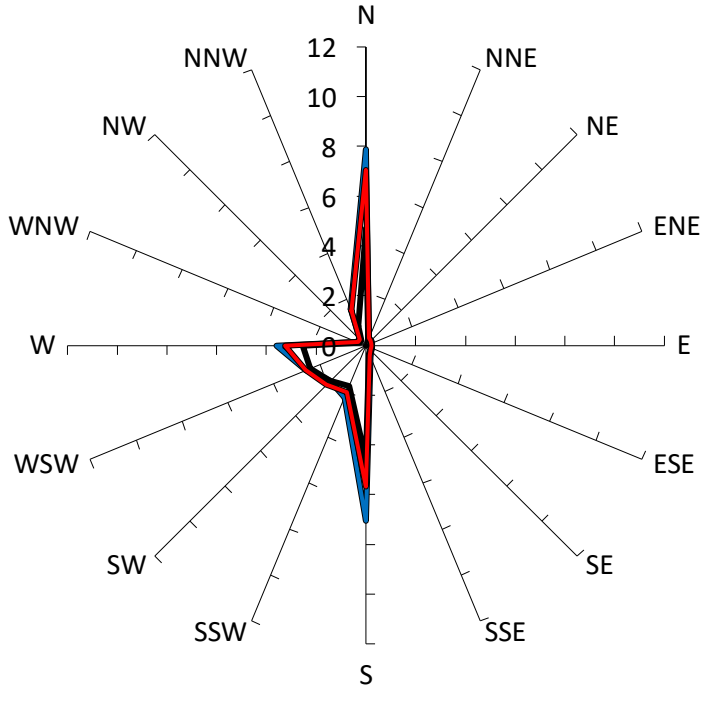


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	32%	31
Existing Site Conditions	5%	14
With the inclusion of the mitigation strategy detailed within the report.	16%	18

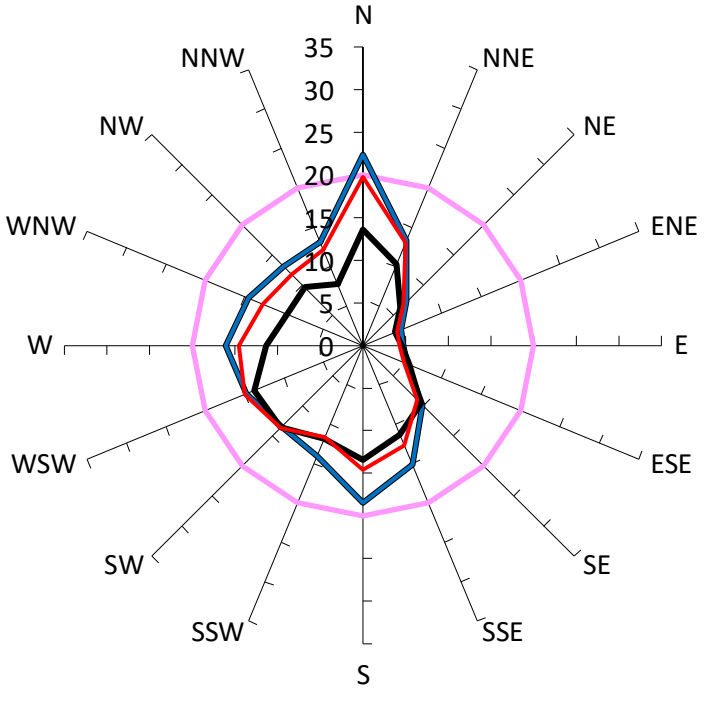
Results for P03

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

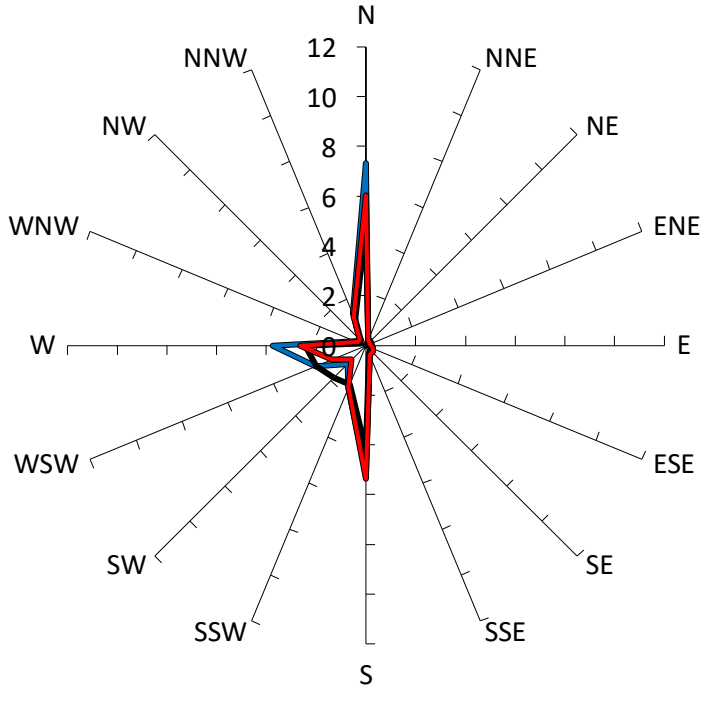


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	31%	22
Existing Site Conditions	8%	14
With the inclusion of the mitigation strategy detailed within the report.	24%	20

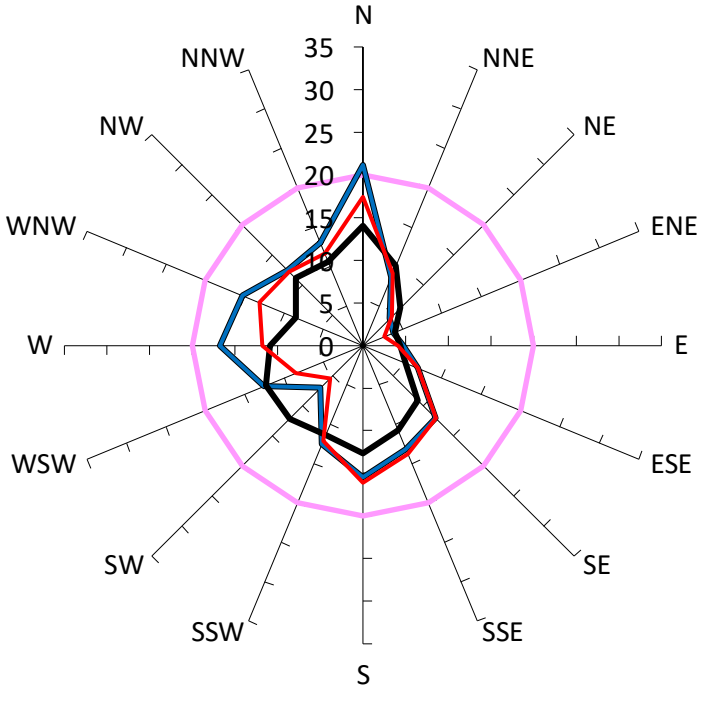
Results for P04

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

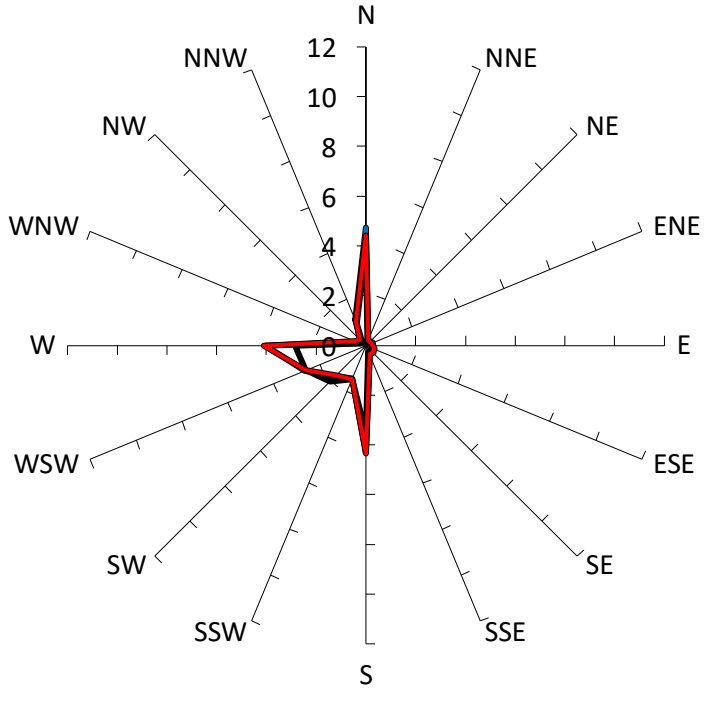


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	21%	21
Existing Site Conditions	7%	14
With the inclusion of the mitigation strategy detailed within the report.	16%	17

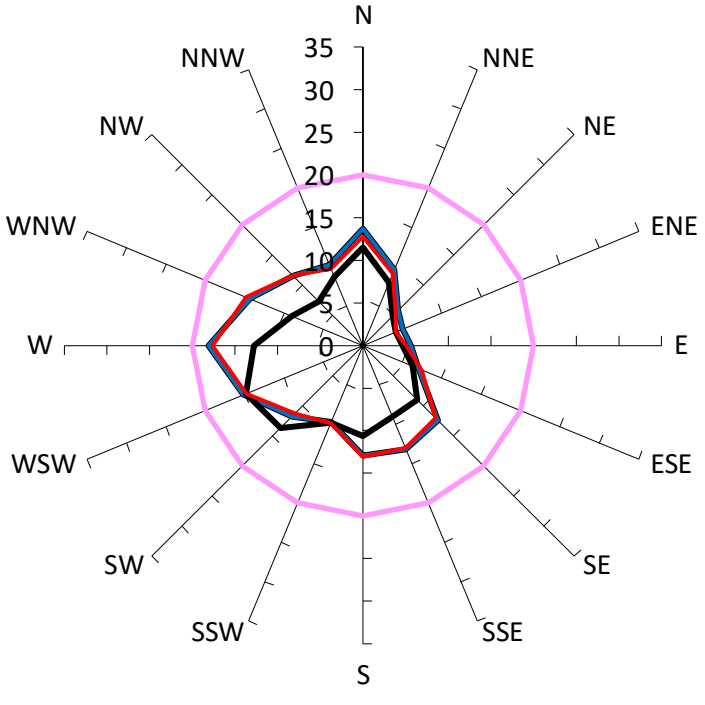
Results for P05

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

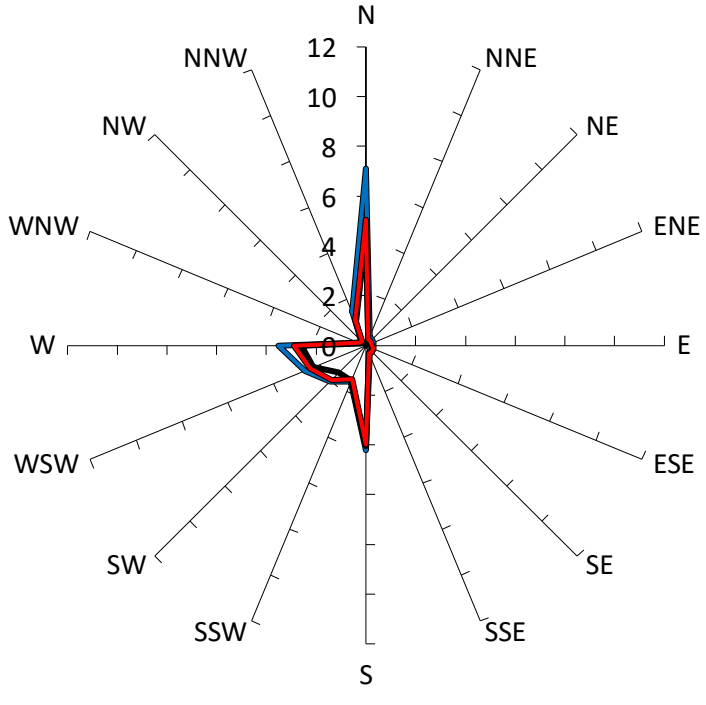


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	14%	18
Existing Site Conditions	4%	15
With the inclusion of the mitigation strategy detailed within the report.	14%	18

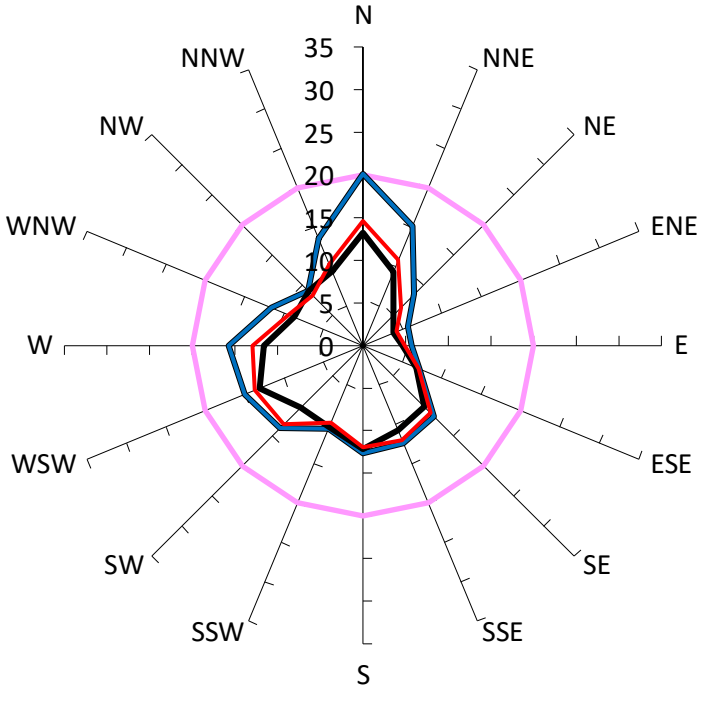
Results for P06

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

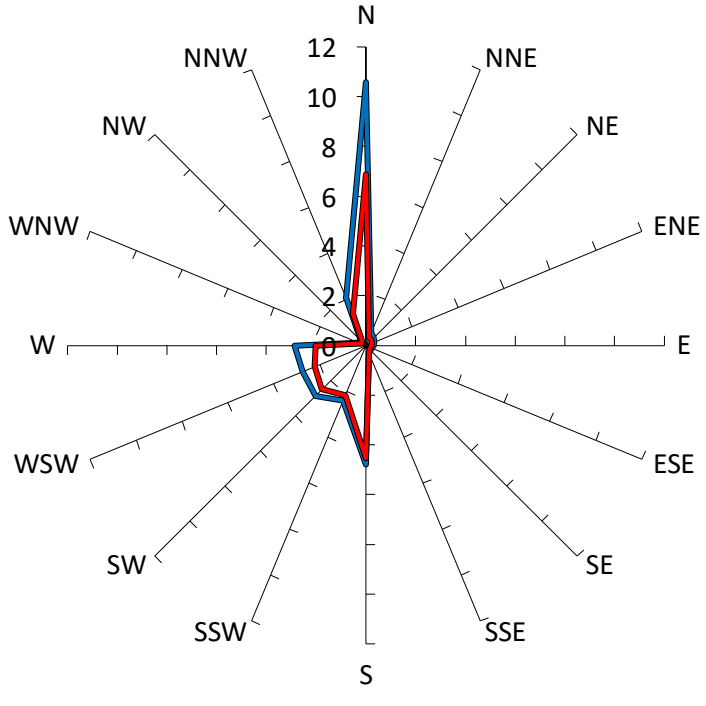


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	19%	20
Existing Site Conditions	5%	13
With the inclusion of the mitigation strategy detailed within the report.	9%	15

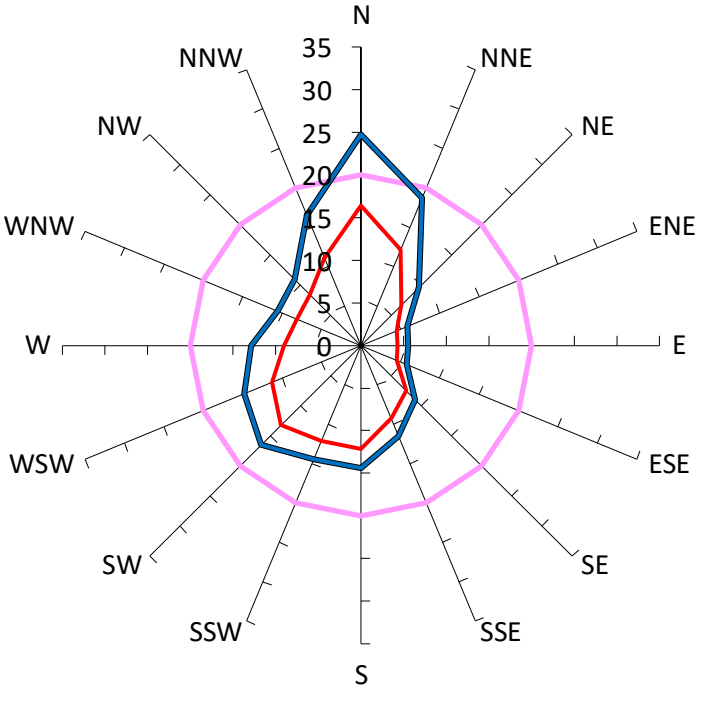
Results for P07

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

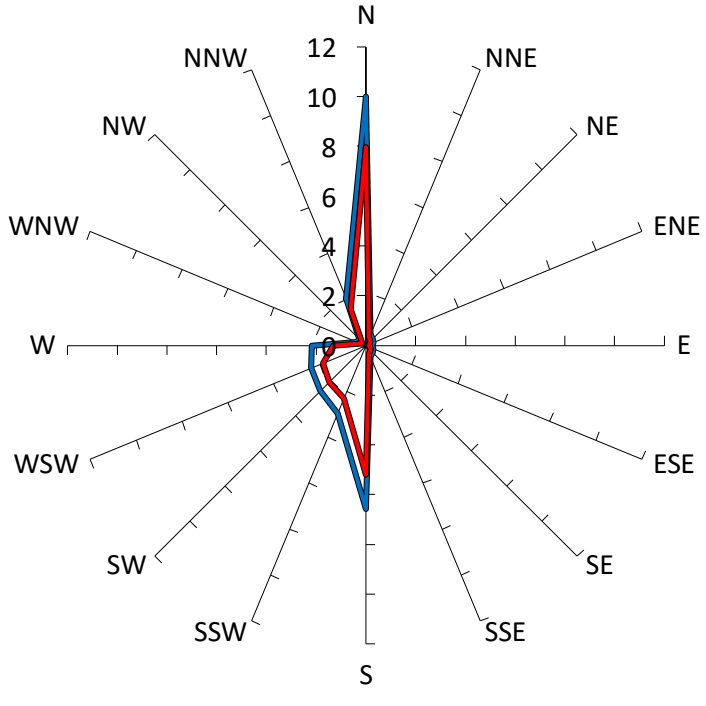


Safety Limit: 20m/s

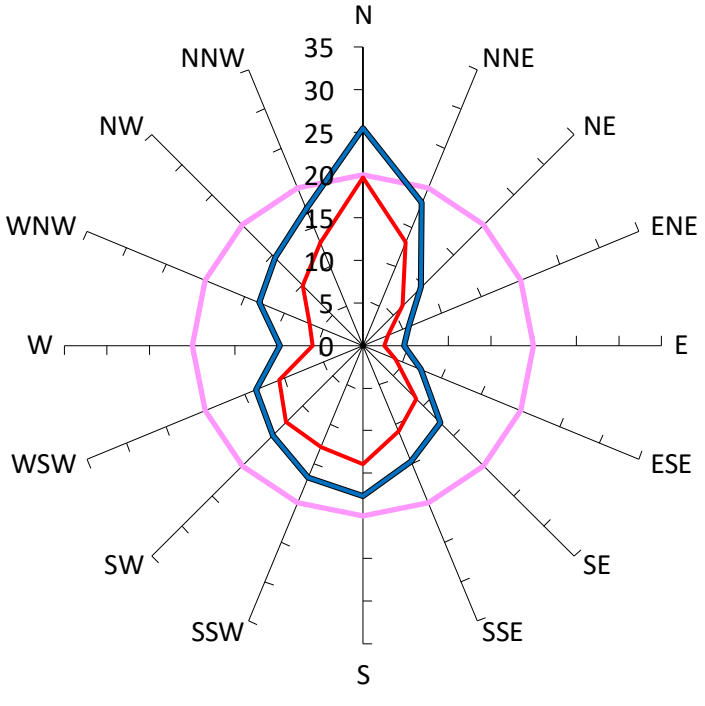
Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	27%	25
With the inclusion of the mitigation strategy detailed within the report.	17%	16

Results for P08

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

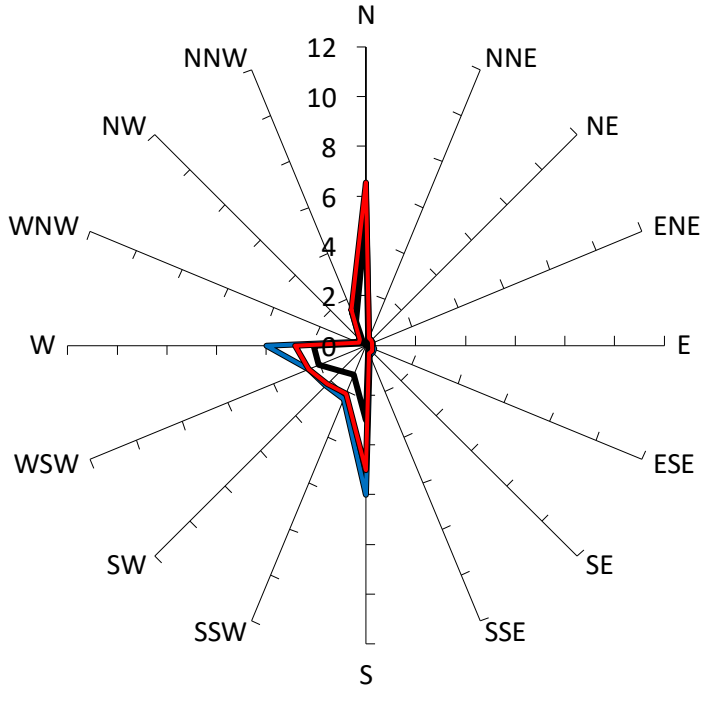


Safety Limit: 20m/s

	Description	GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
	With development "as proposed", no vegetation or other treatments.	34%	25
	With the inclusion of the mitigation strategy detailed within the report.	20%	20

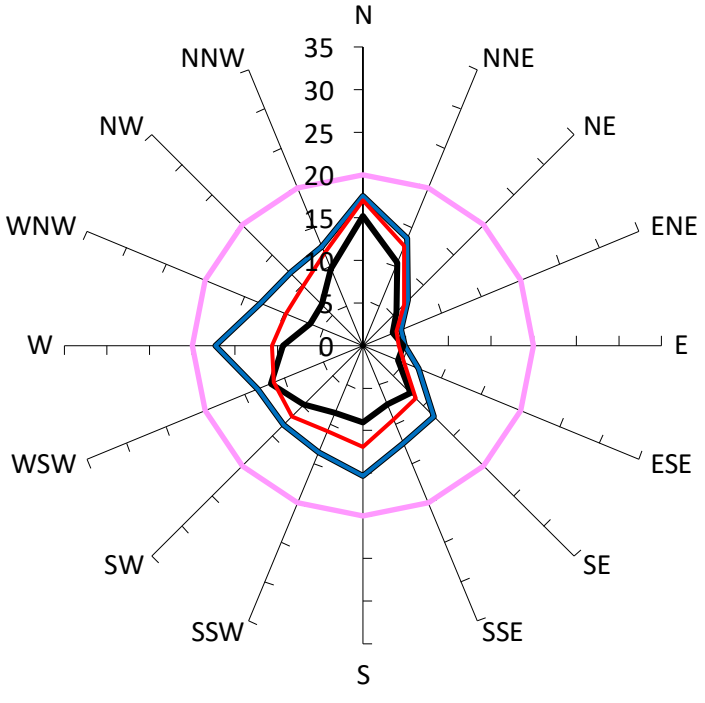
Results for P09

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

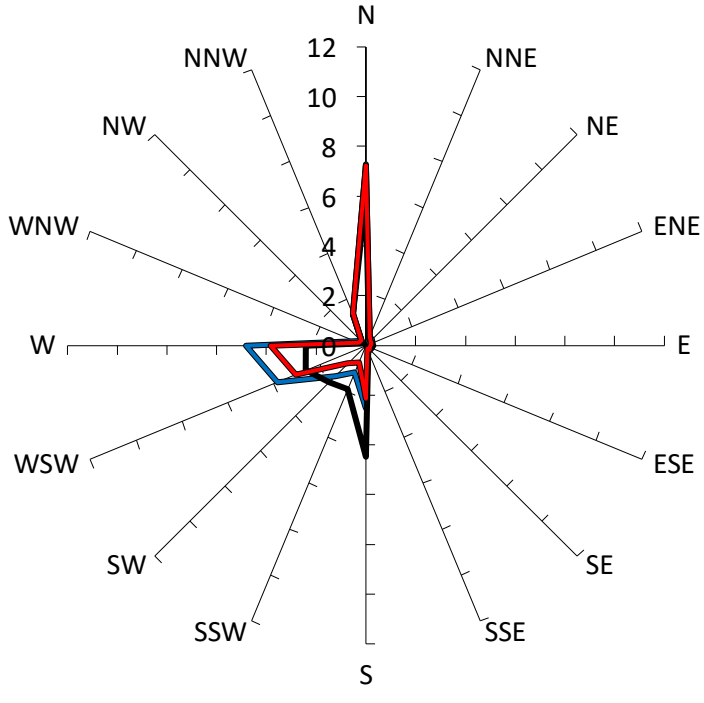


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	27%	18
Existing Site Conditions	7%	15
With the inclusion of the mitigation strategy detailed within the report.	19%	17

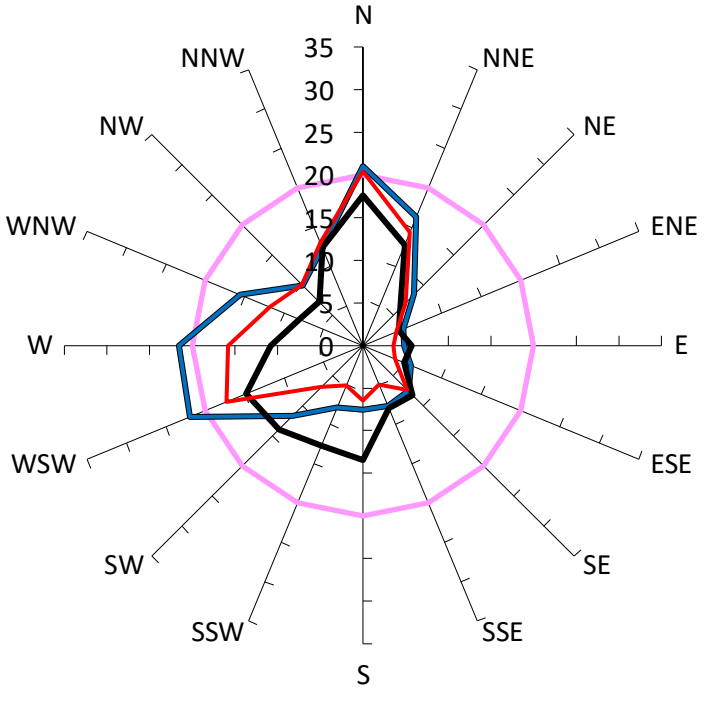
Results for P10

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

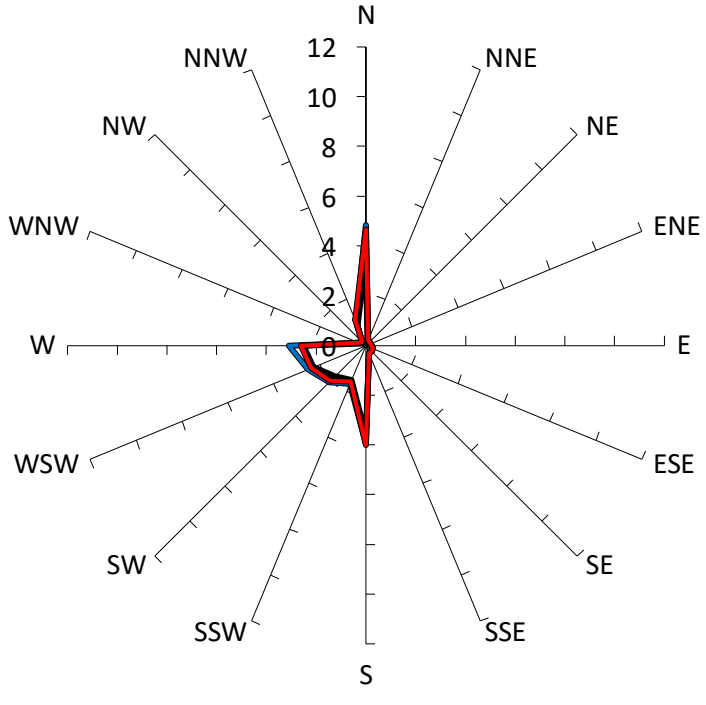


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	24%	22
Existing Site Conditions	14%	18
With the inclusion of the mitigation strategy detailed within the report.	20%	20

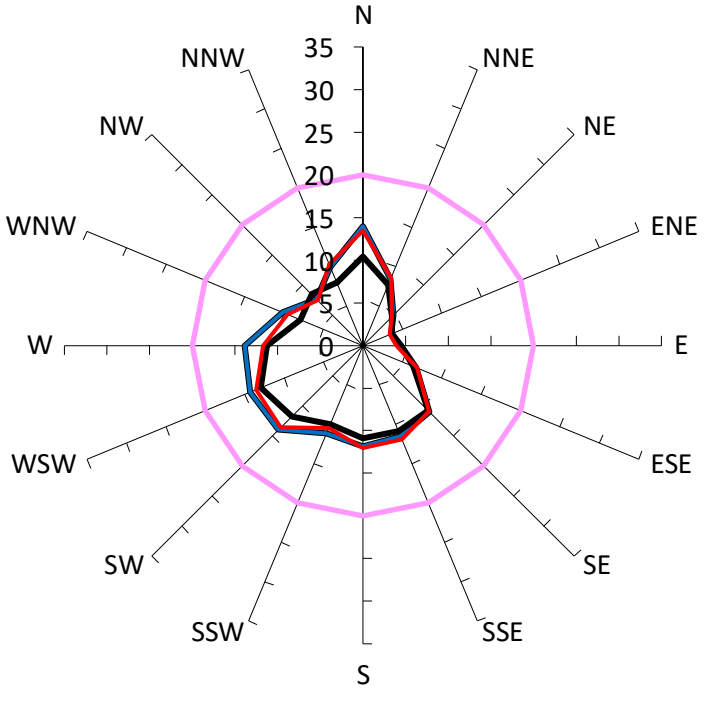
Results for P11

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

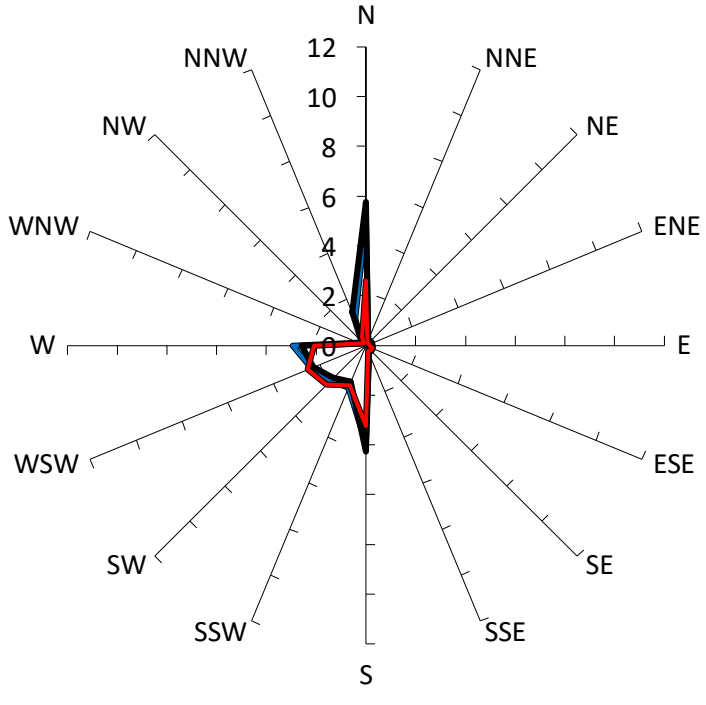


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	9%	14
Existing Site Conditions	3%	13
With the inclusion of the mitigation strategy detailed within the report.	7%	14

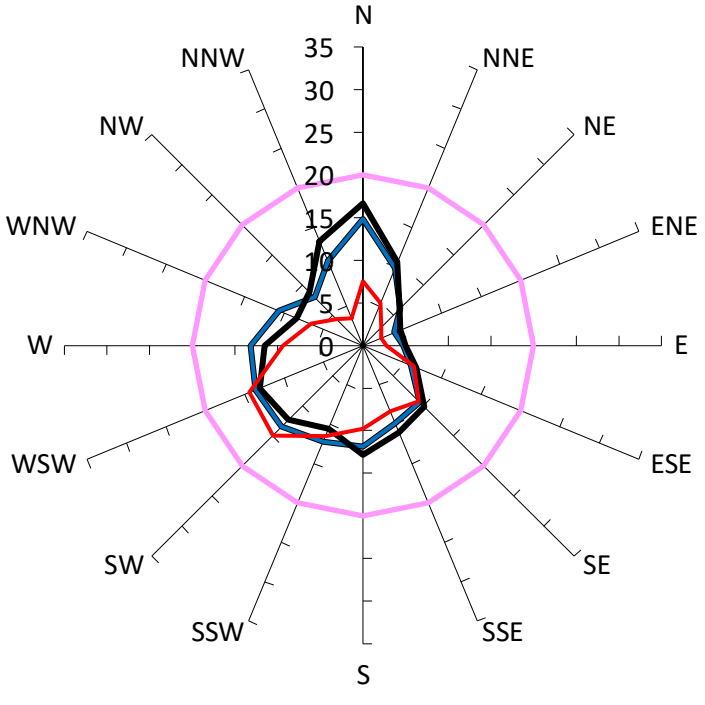
Results for P12

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

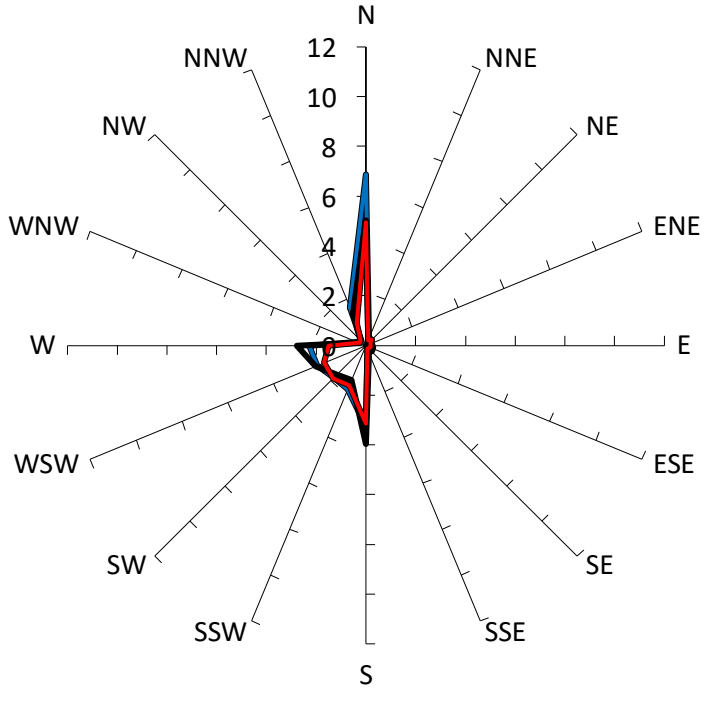


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	10%	15
Existing Site Conditions	13%	17
With the inclusion of the mitigation strategy detailed within the report.	3%	15

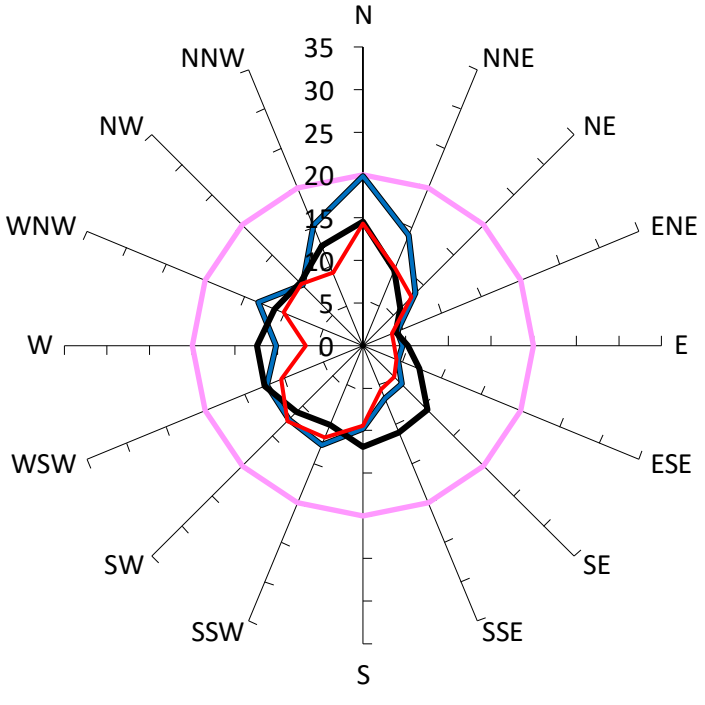
Results for P13

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

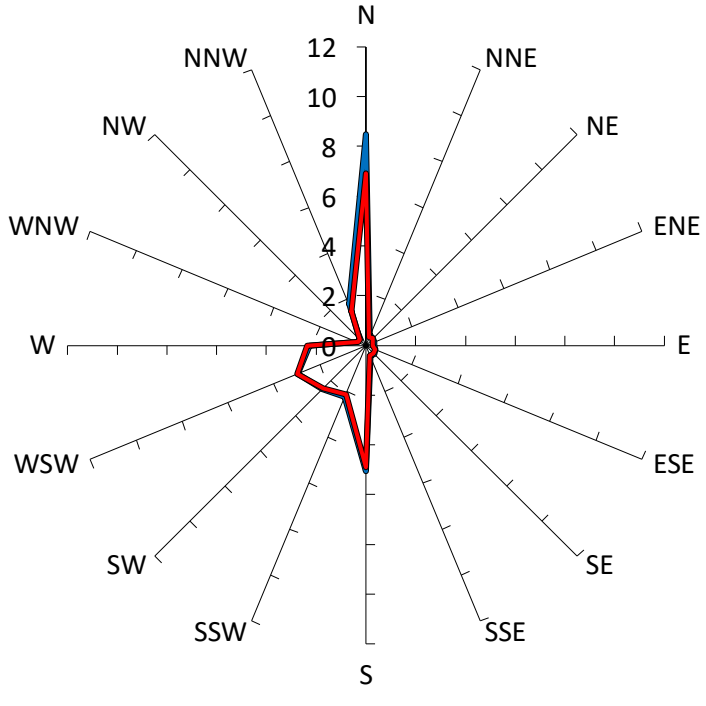


Safety Limit: 20m/s

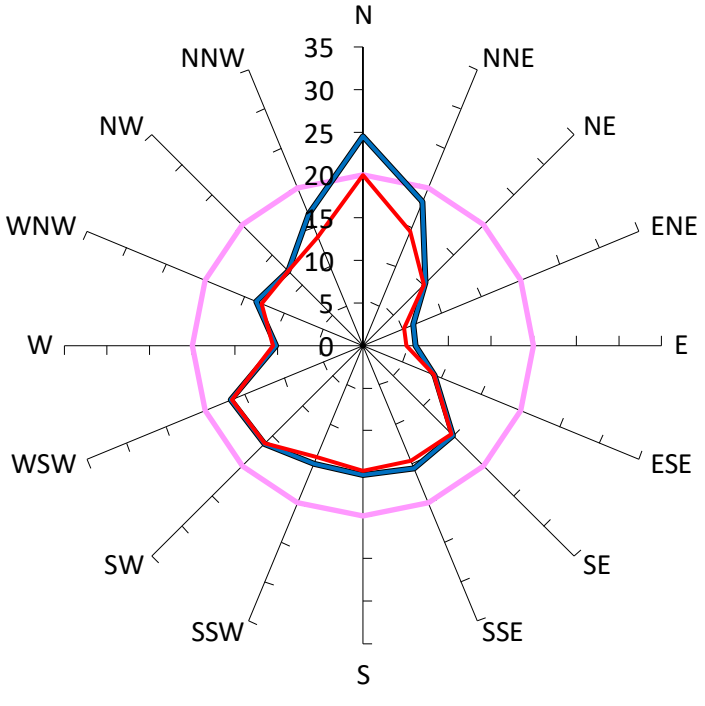
Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	16%	20
Existing Site Conditions	9%	15
With the inclusion of the mitigation strategy detailed within the report.	6%	14

Results for P14

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

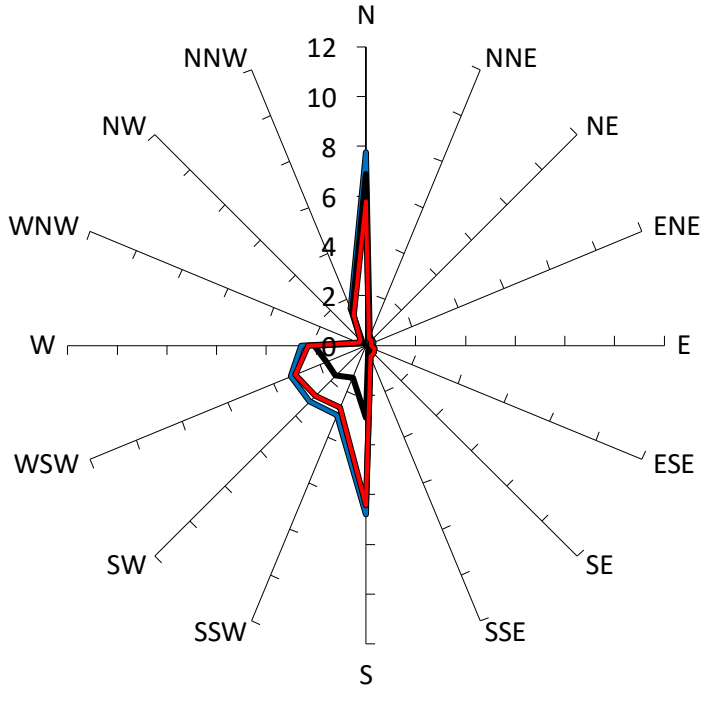


Safety Limit: 20m/s

	Description	GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
	With development "as proposed", no vegetation or other treatments.	27%	25
	With the inclusion of the mitigation strategy detailed within the report.	22%	20

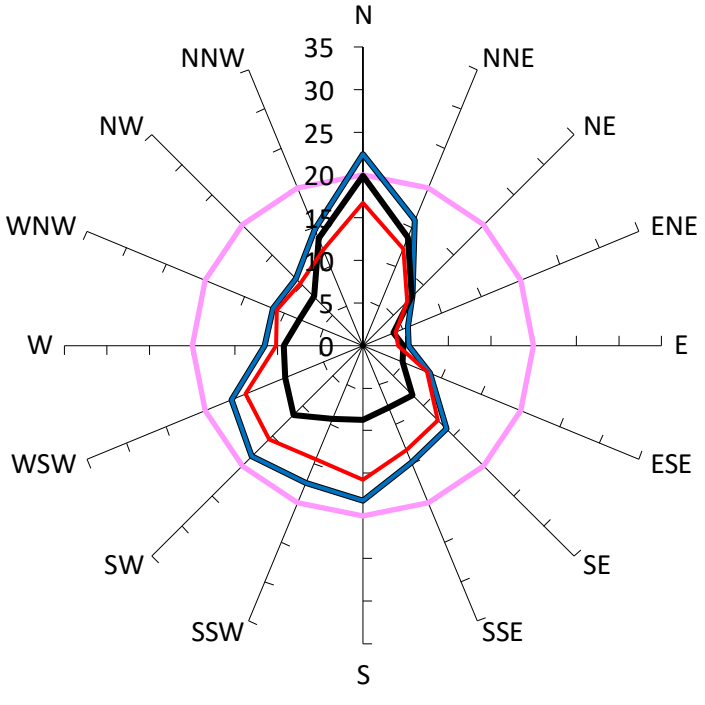
Results for P15

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

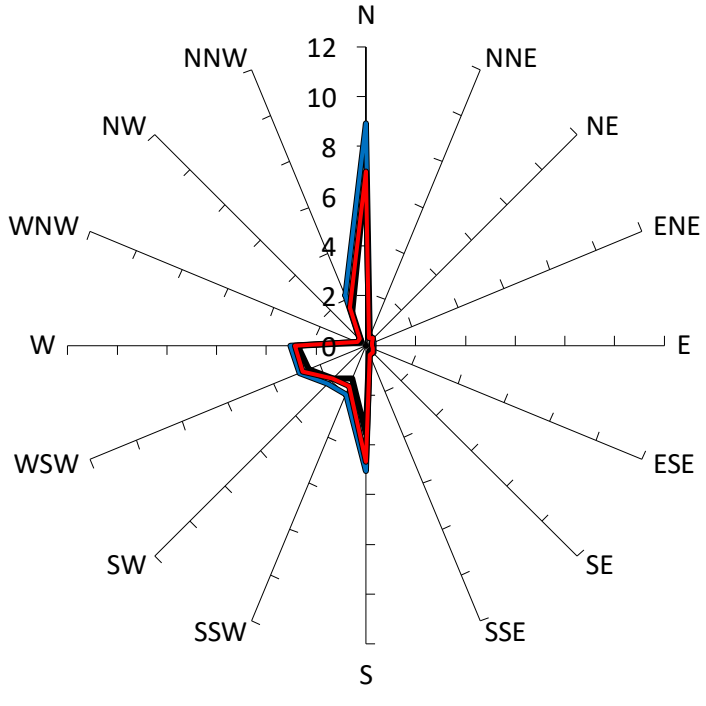


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	34%	22
Existing Site Conditions	13%	20
With the inclusion of the mitigation strategy detailed within the report.	29%	17

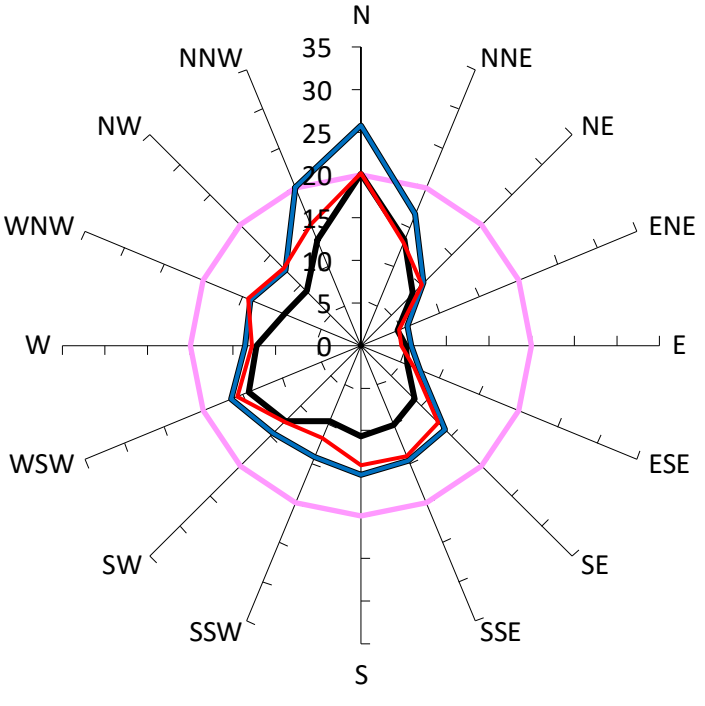
Results for P16

Gust Equivalent Mean (m/s)



Comfort Criteria: 4m/s with 20% probability of exceedence

Maximum Gust (m/s)

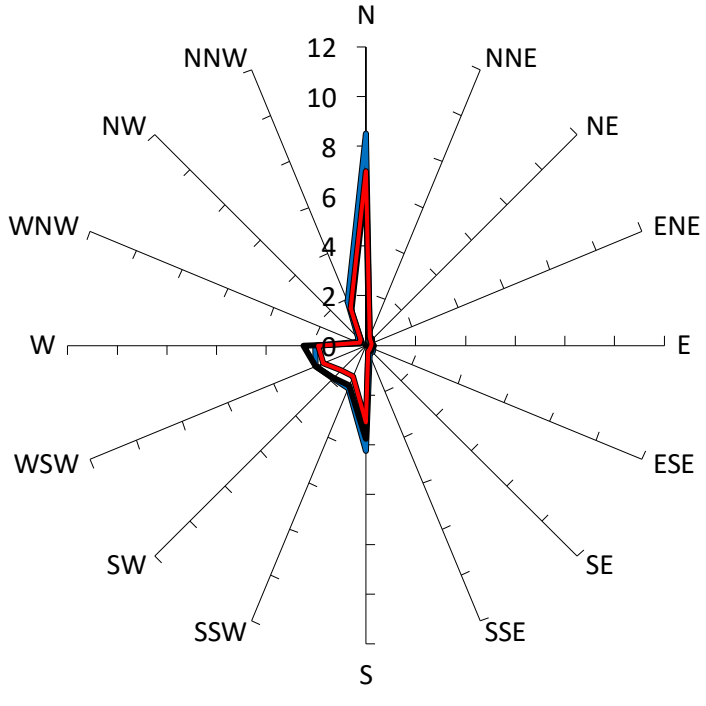


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Sitting comfort (4m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	42%	26
Existing Site Conditions	25%	20
With the inclusion of the mitigation strategy detailed within the report.	35%	20

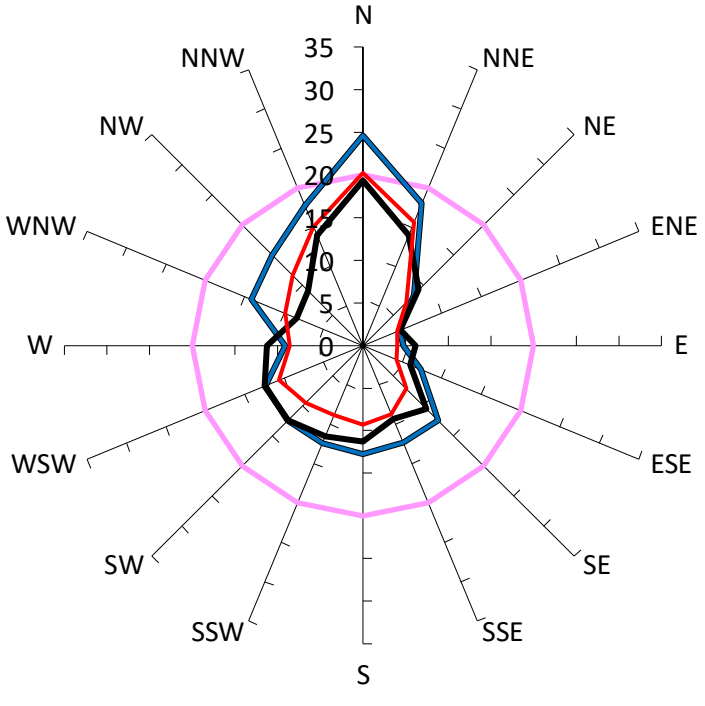
Results for P17

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

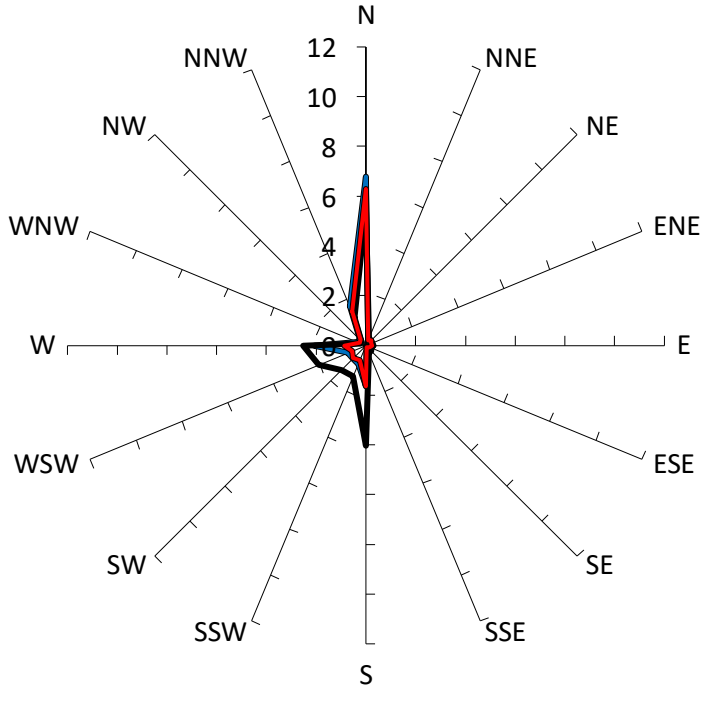


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	21%	25
Existing Site Conditions	14%	19
With the inclusion of the mitigation strategy detailed within the report.	15%	20

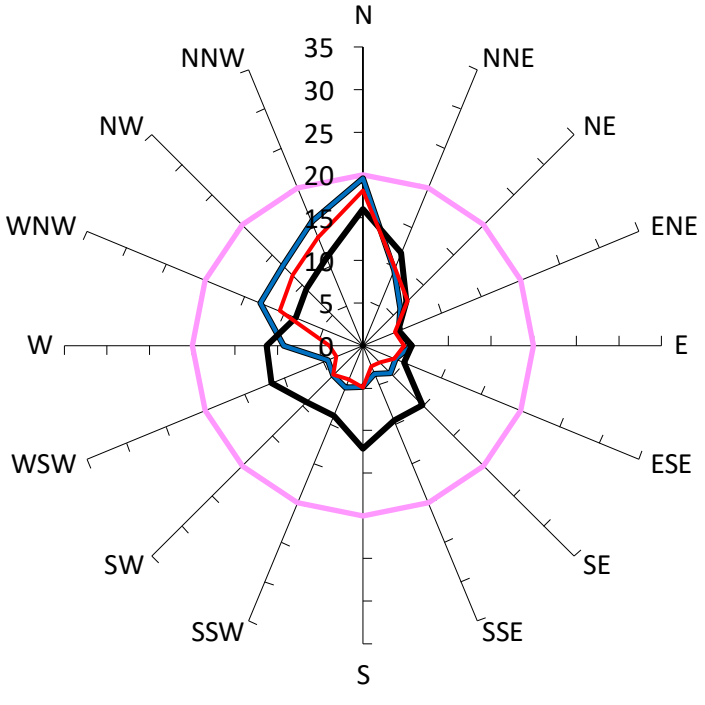
Results for P18

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

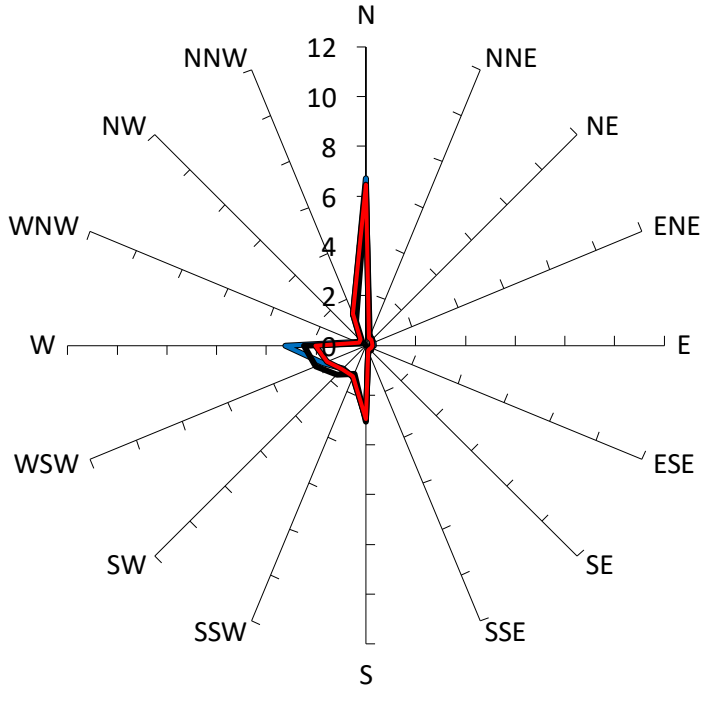


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	14%	20
Existing Site Conditions	11%	16
With the inclusion of the mitigation strategy detailed within the report.	11%	18

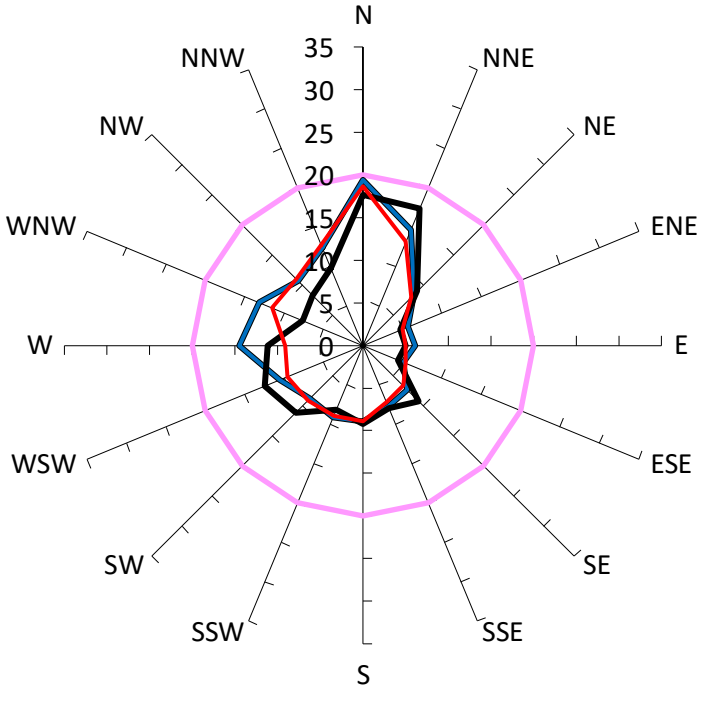
Results for P19

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

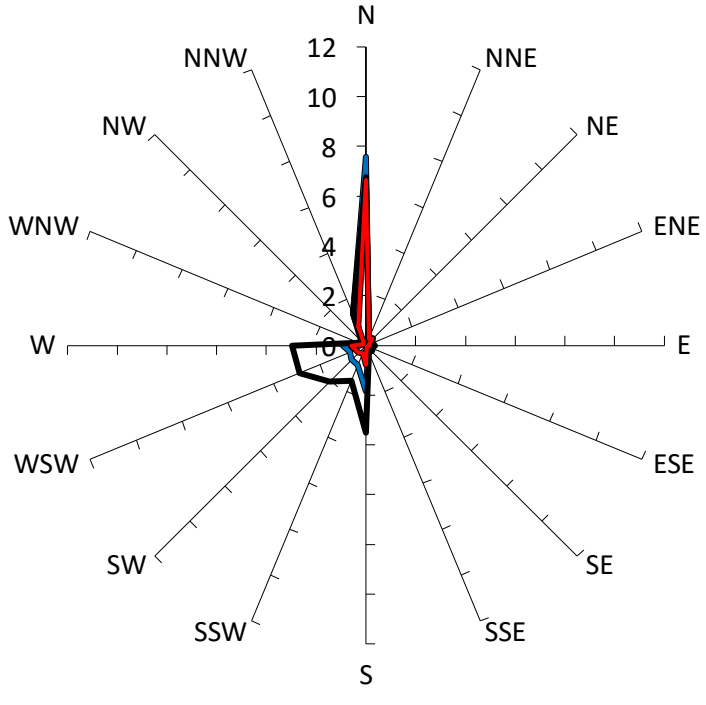


Safety Limit: 20m/s

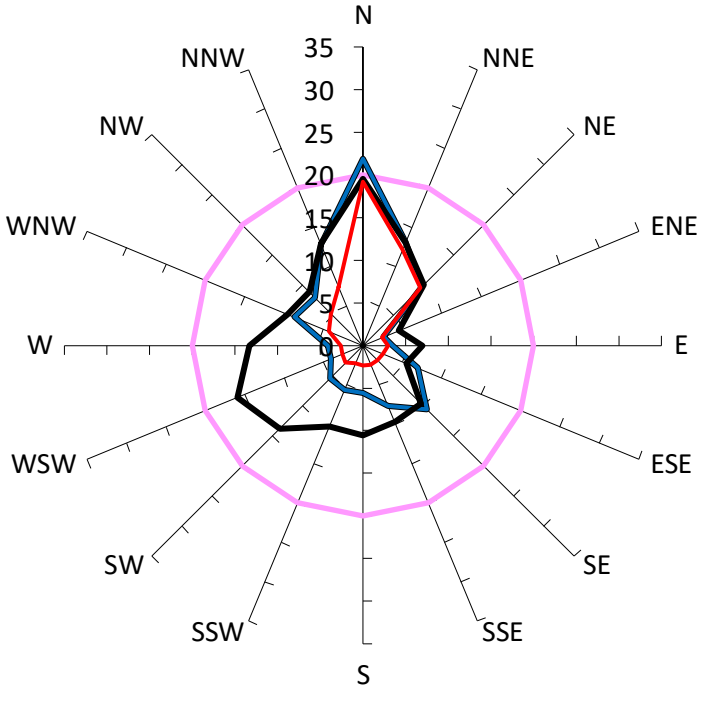
Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	15%	19
Existing Site Conditions	12%	18
With the inclusion of the mitigation strategy detailed within the report.	12%	19

Results for P20

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

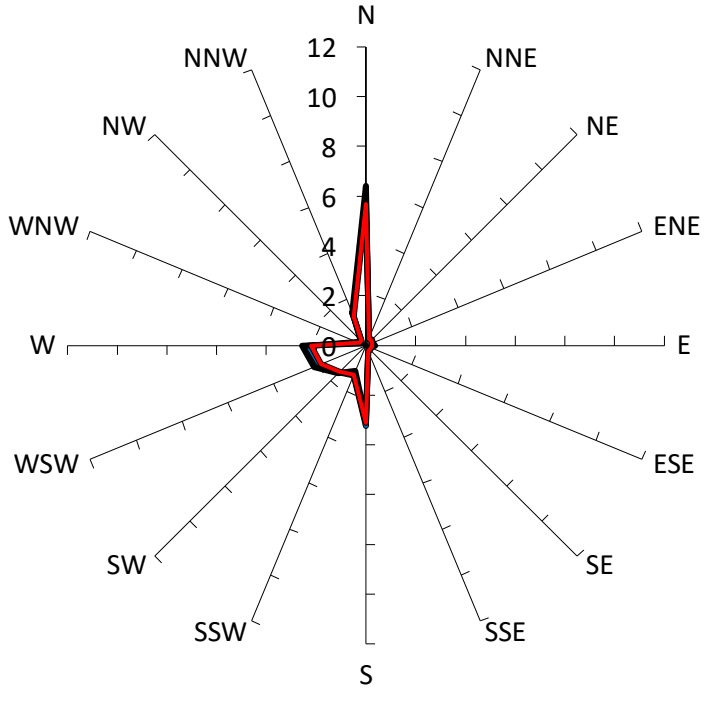


Safety Limit: 20m/s

	Description	GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
	With development "as proposed", no vegetation or other treatments.	13%	22
	Existing Site Conditions	16%	20
	With the inclusion of the mitigation strategy detailed within the report.	10%	19

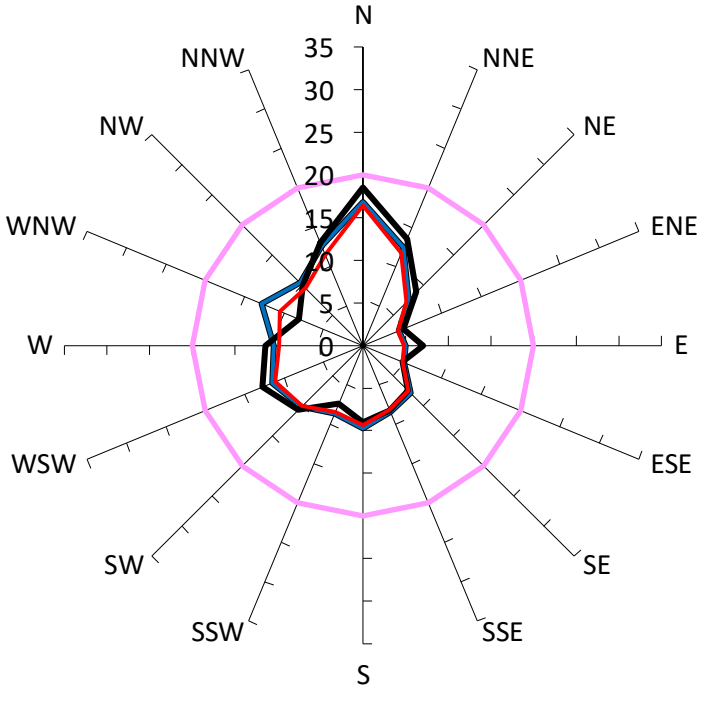
Results for P21

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

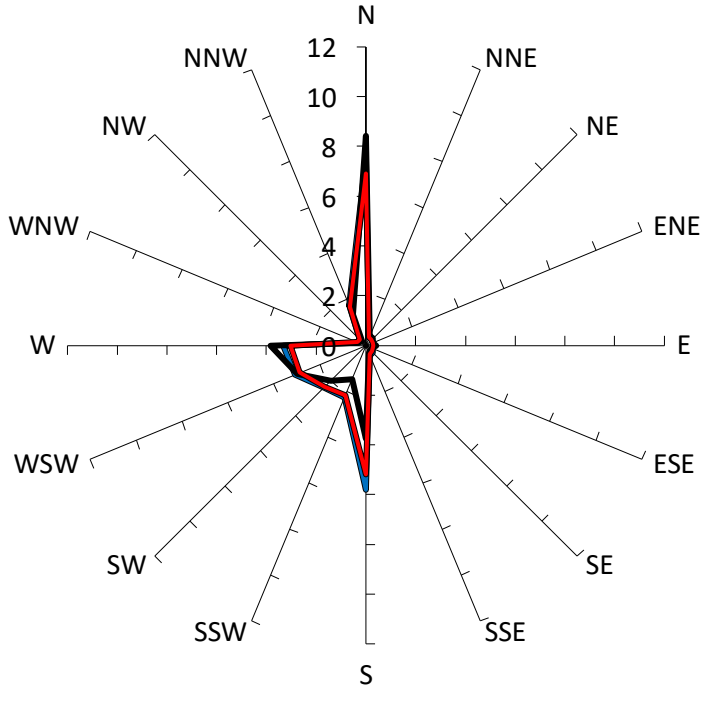


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	12%	17
Existing Site Conditions	13%	19
With the inclusion of the mitigation strategy detailed within the report.	10%	16

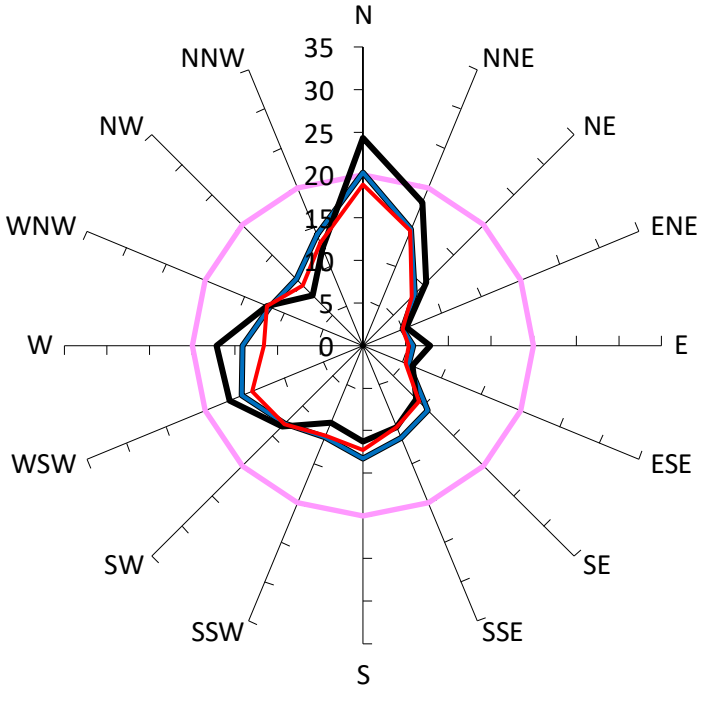
Results for P22

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

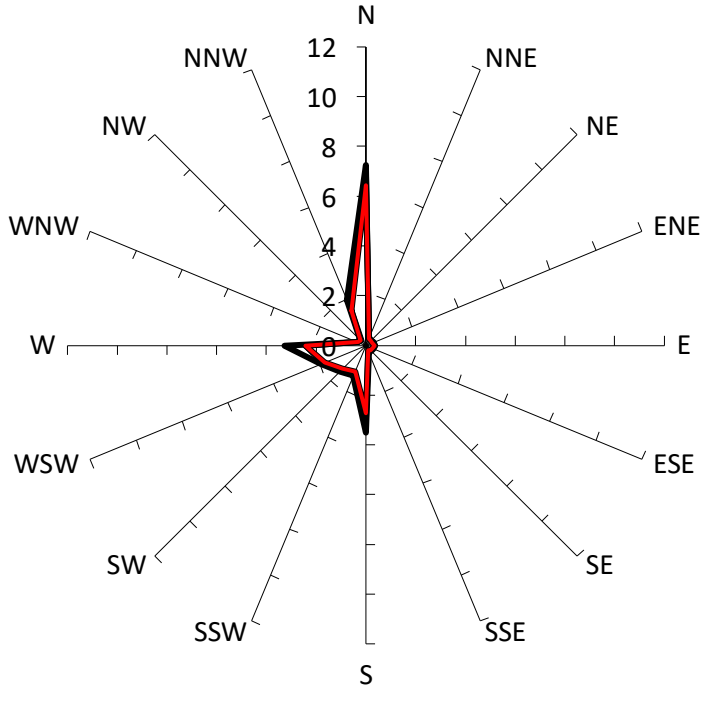


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	28%	20
Existing Site Conditions	22%	24
With the inclusion of the mitigation strategy detailed within the report.	23%	19

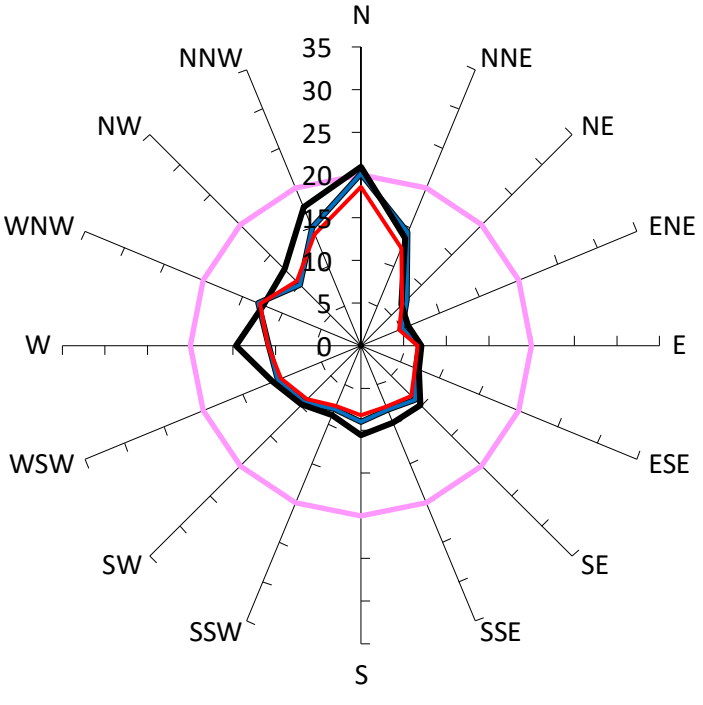
Results for P23

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

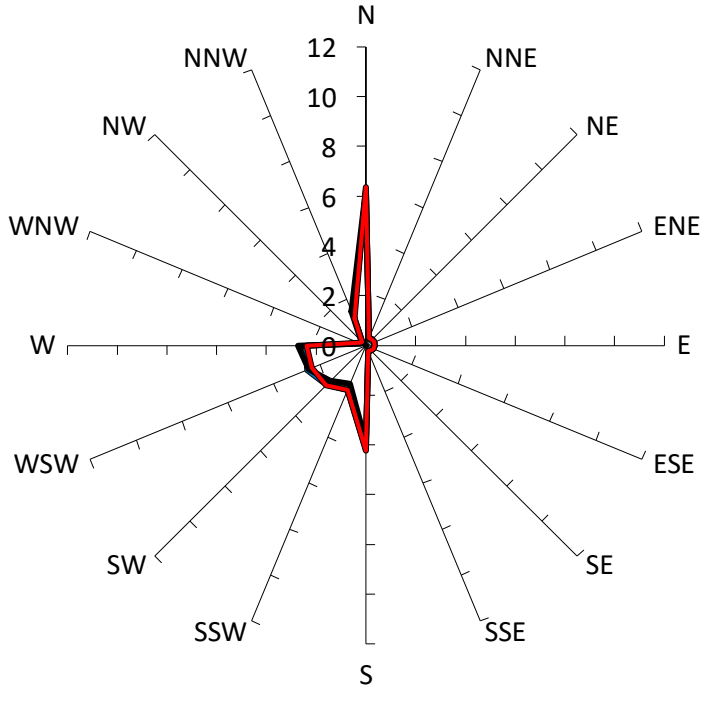


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	15%	20
Existing Site Conditions	18%	21
With the inclusion of the mitigation strategy detailed within the report.	13%	19

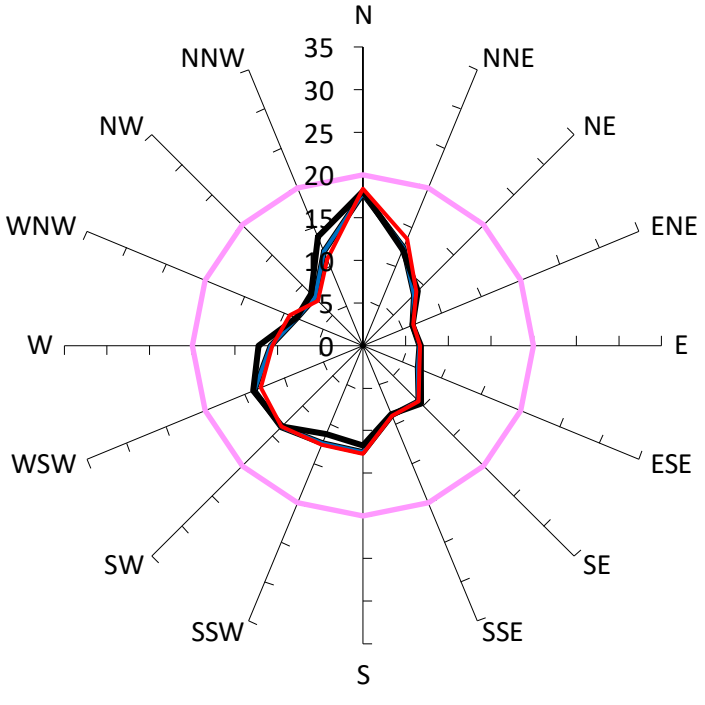
Results for P24

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

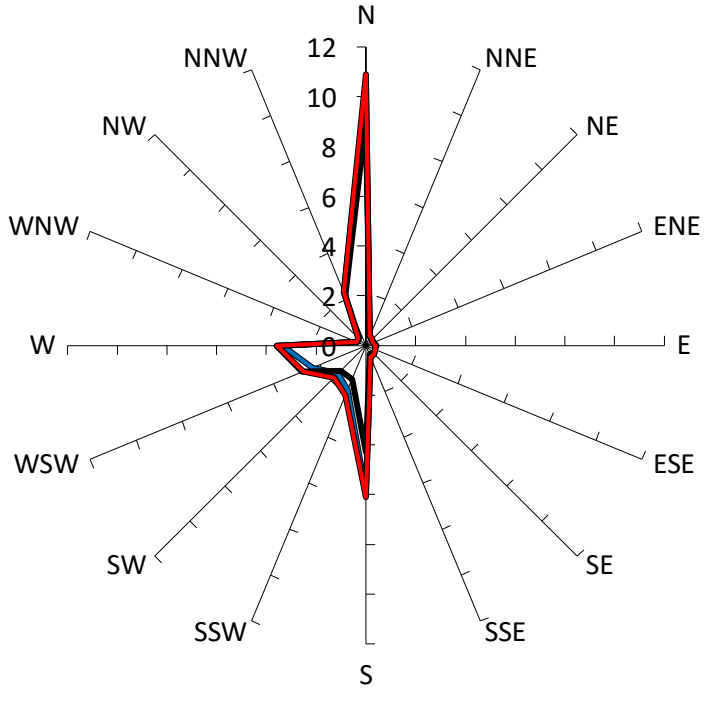


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	14%	18
Existing Site Conditions	14%	18
With the inclusion of the mitigation strategy detailed within the report.	14%	18

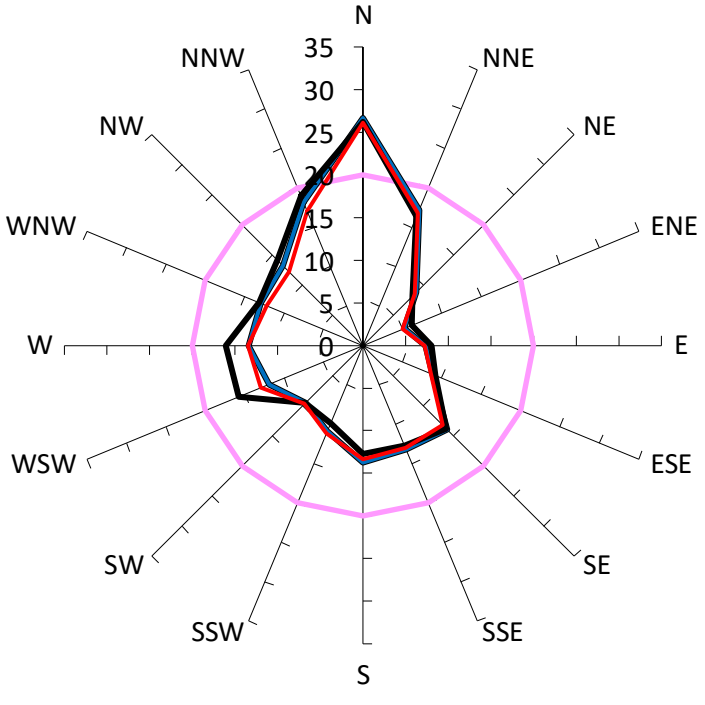
Results for P25

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

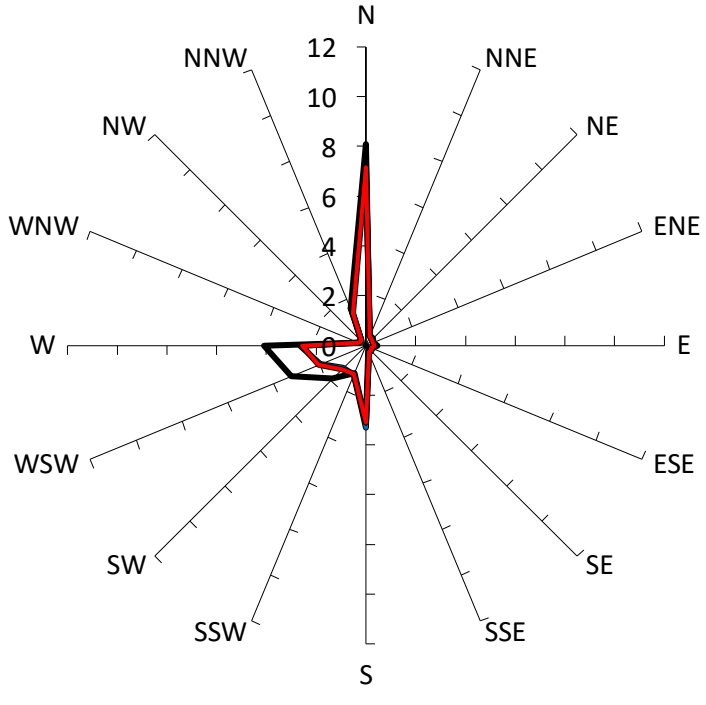


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	31%	27
Existing Site Conditions	25%	26
With the inclusion of the mitigation strategy detailed within the report.	34%	26

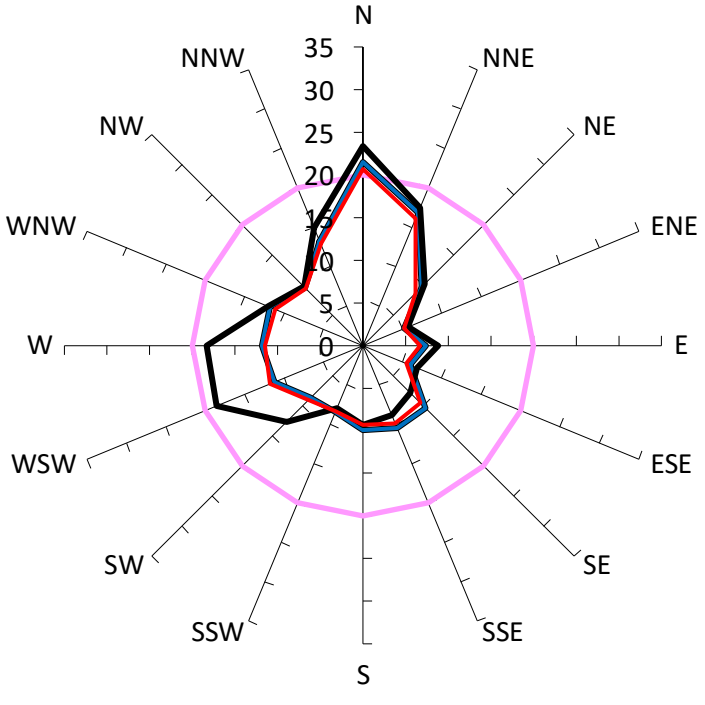
Results for P26

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

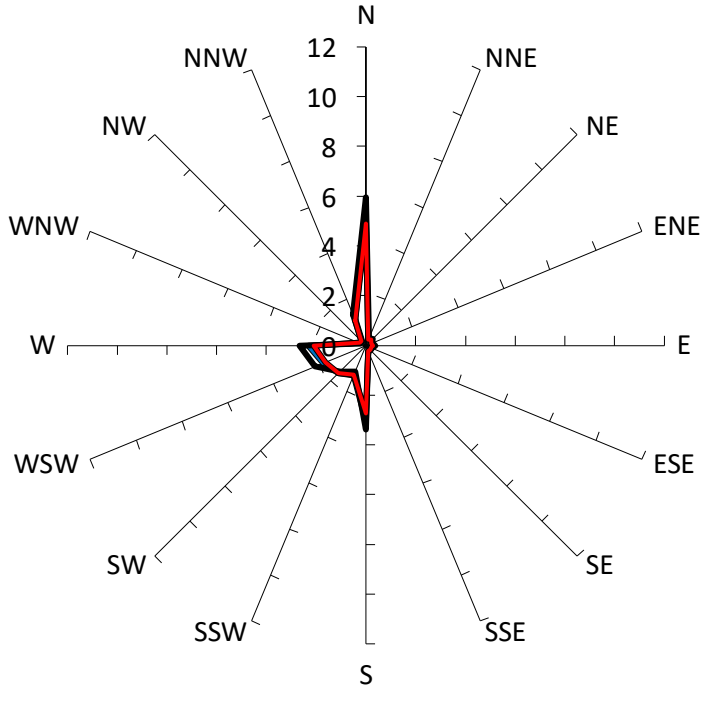


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	15%	22
Existing Site Conditions	24%	23
With the inclusion of the mitigation strategy detailed within the report.	14%	21

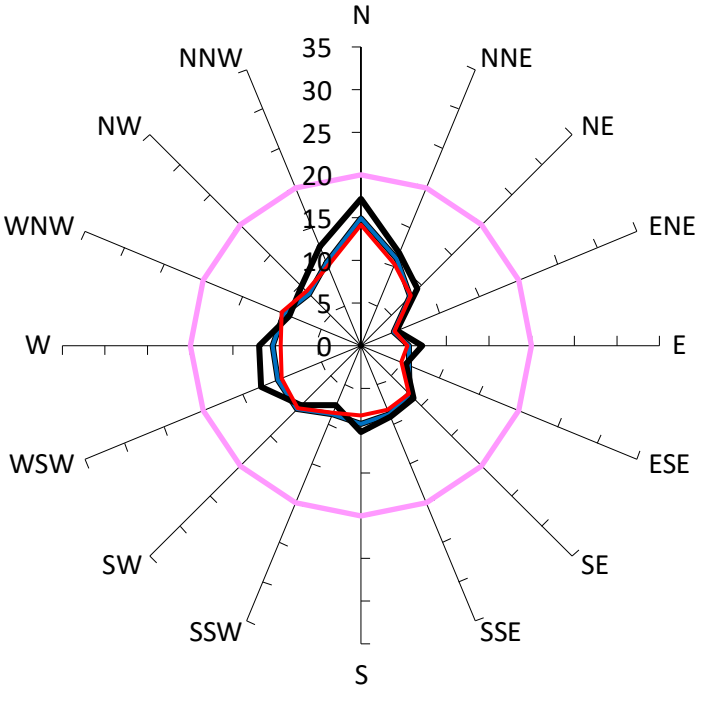
Results for P27

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

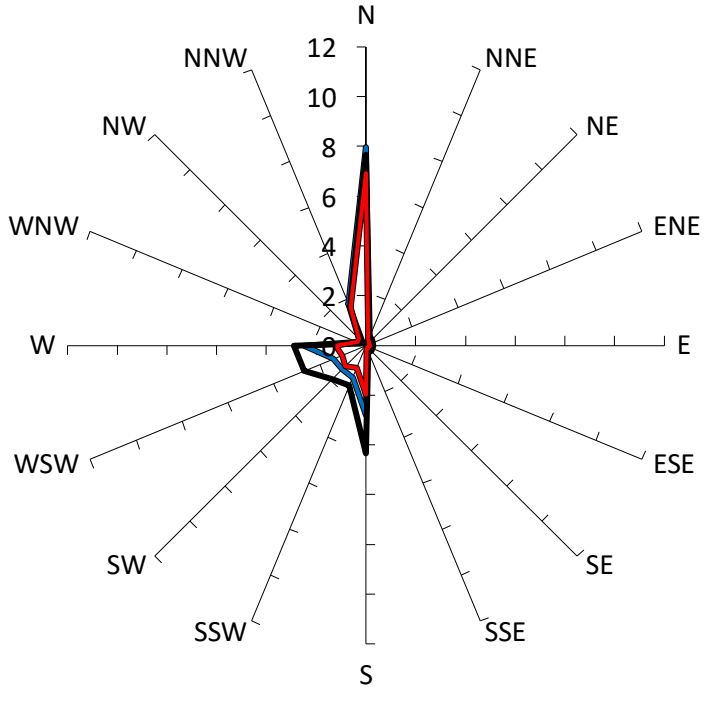


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	7%	15
Existing Site Conditions	12%	17
With the inclusion of the mitigation strategy detailed within the report.	5%	14

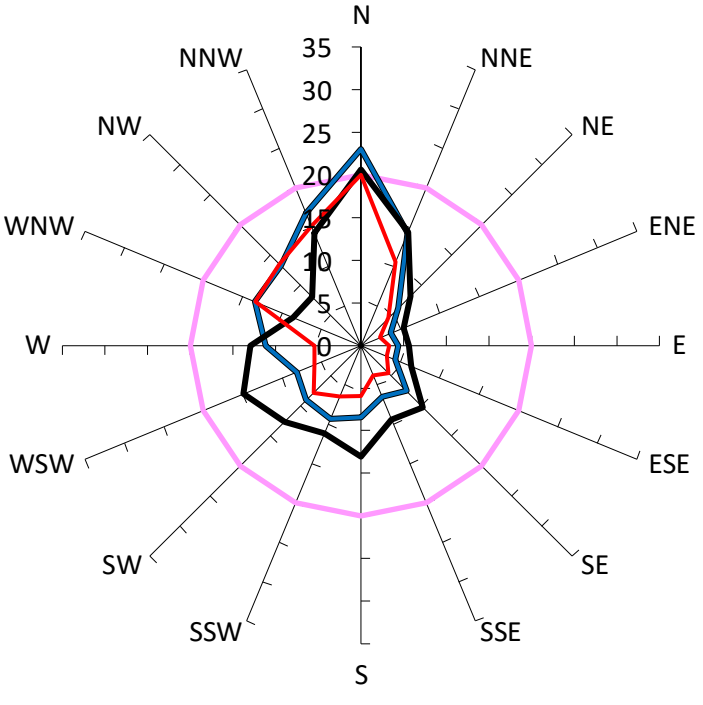
Results for P28

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

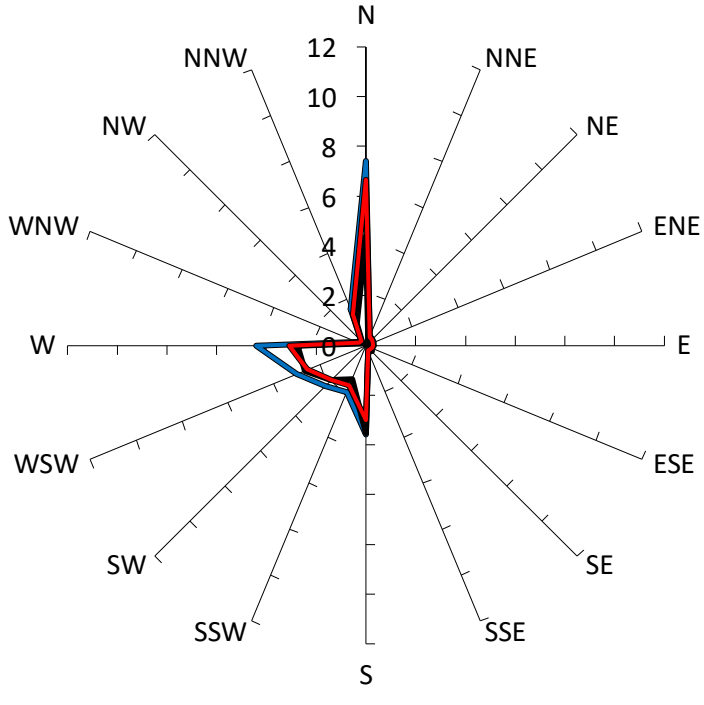


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	17%	23
Existing Site Conditions	19%	21
With the inclusion of the mitigation strategy detailed within the report.	14%	20

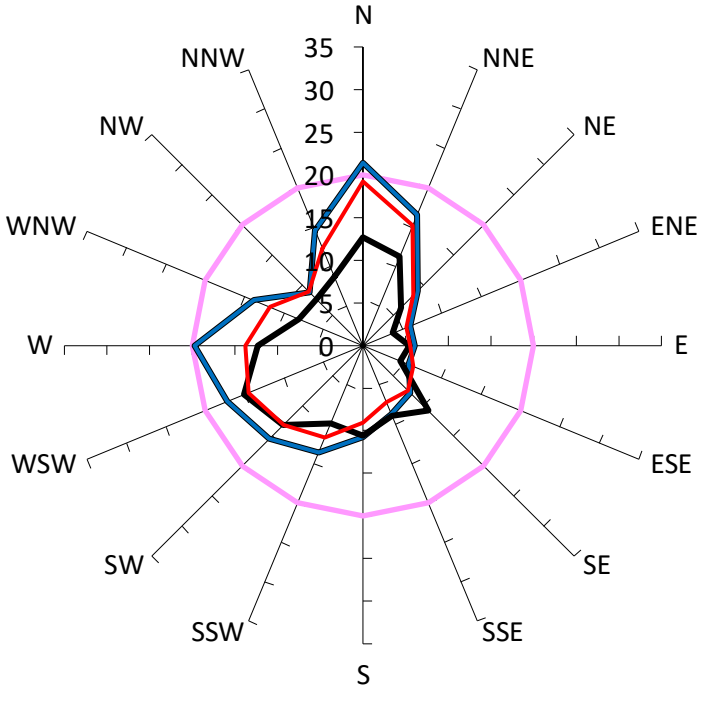
Results for P29

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

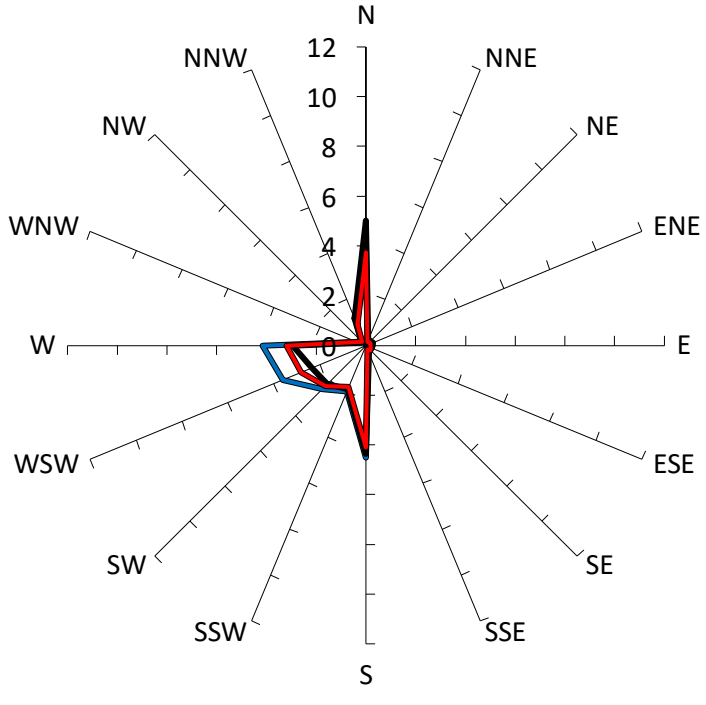


Safety Limit: 20m/s

	Description	GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
	With development "as proposed", no vegetation or other treatments.	24%	21
	Existing Site Conditions	6%	15
	With the inclusion of the mitigation strategy detailed within the report.	16%	19

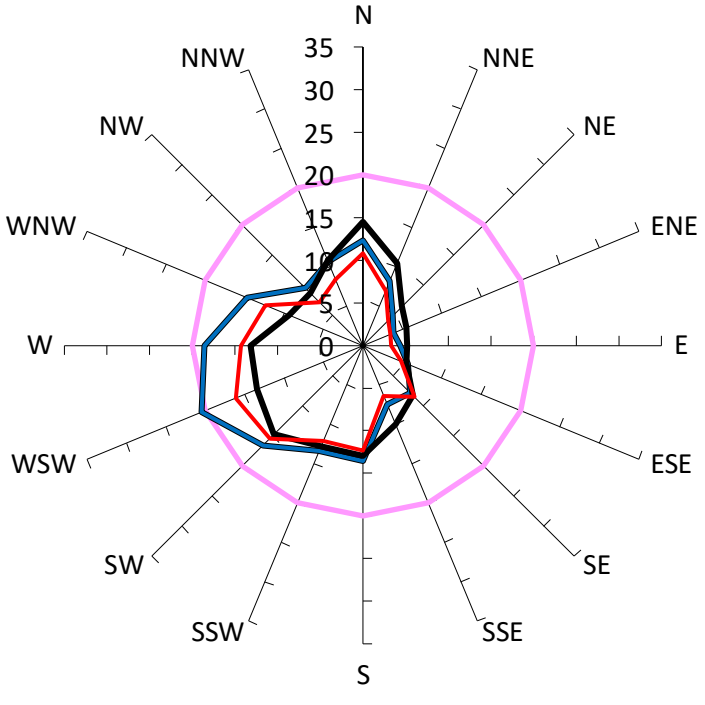
Results for P30

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

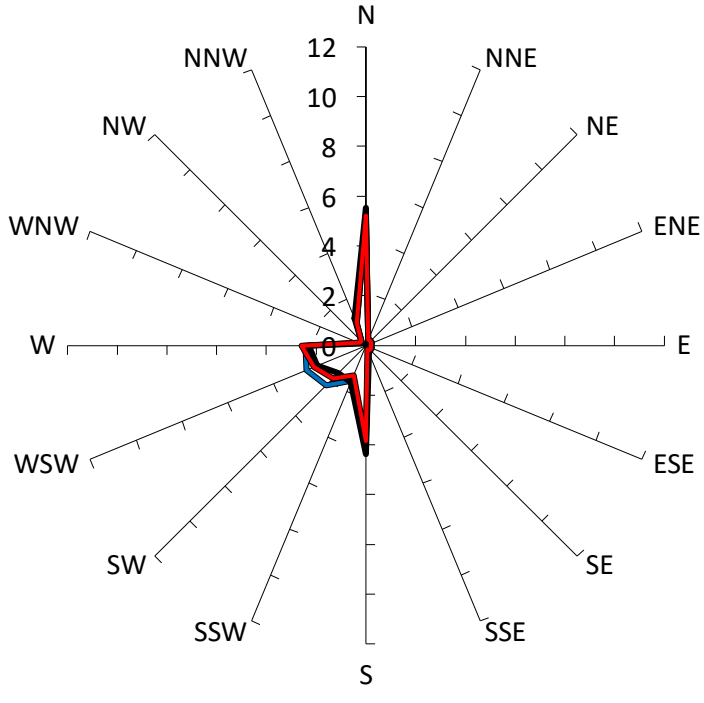


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	16%	20
Existing Site Conditions	10%	15
With the inclusion of the mitigation strategy detailed within the report.	7%	16

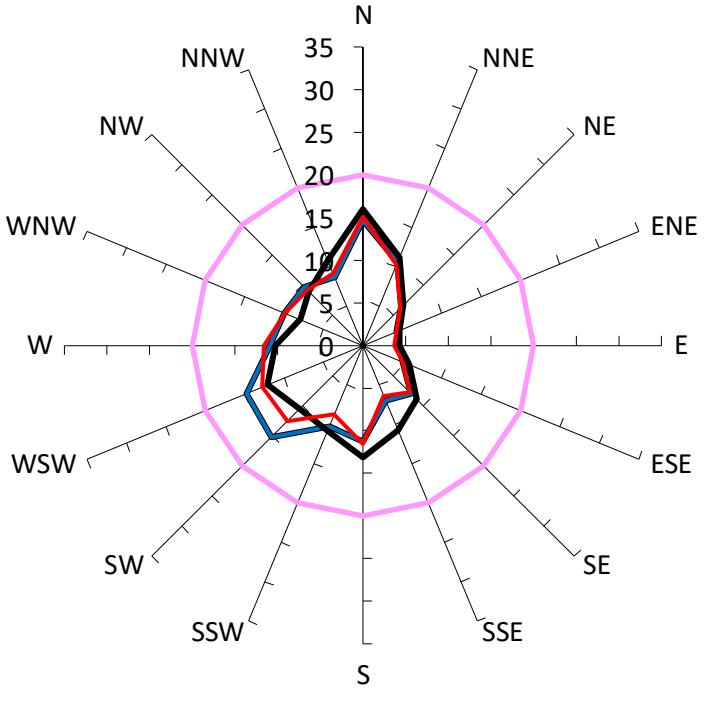
Results for P31

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

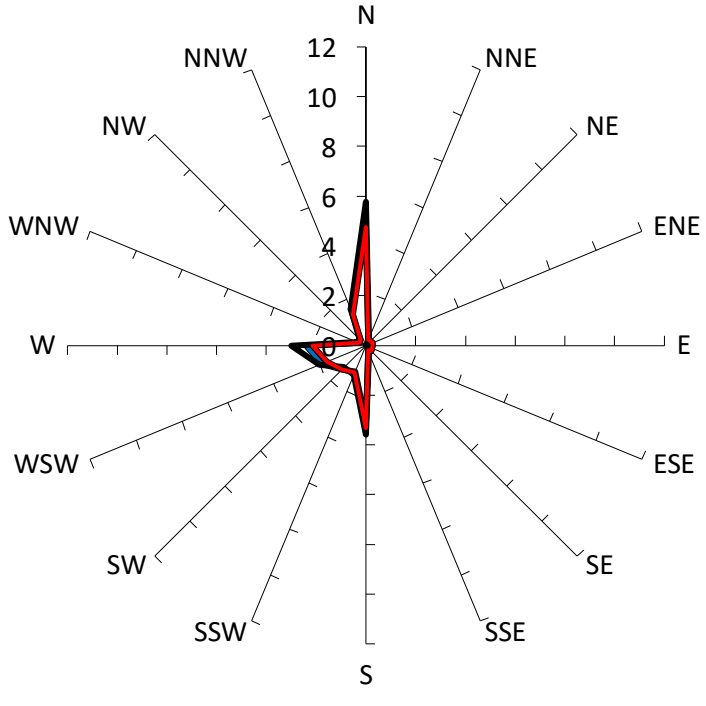


Safety Limit: 20m/s

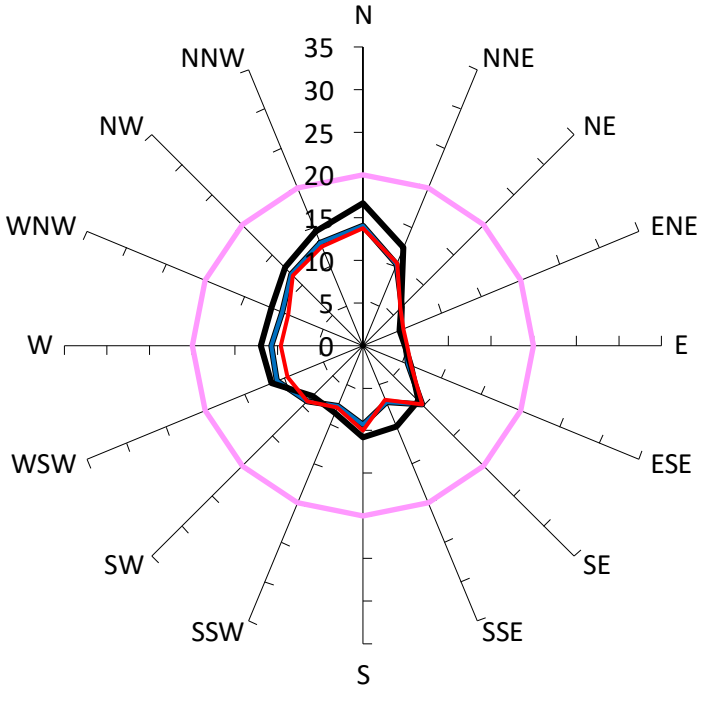
Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	9%	15
Existing Site Conditions	11%	16
With the inclusion of the mitigation strategy detailed within the report.	8%	15

Results for P32

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

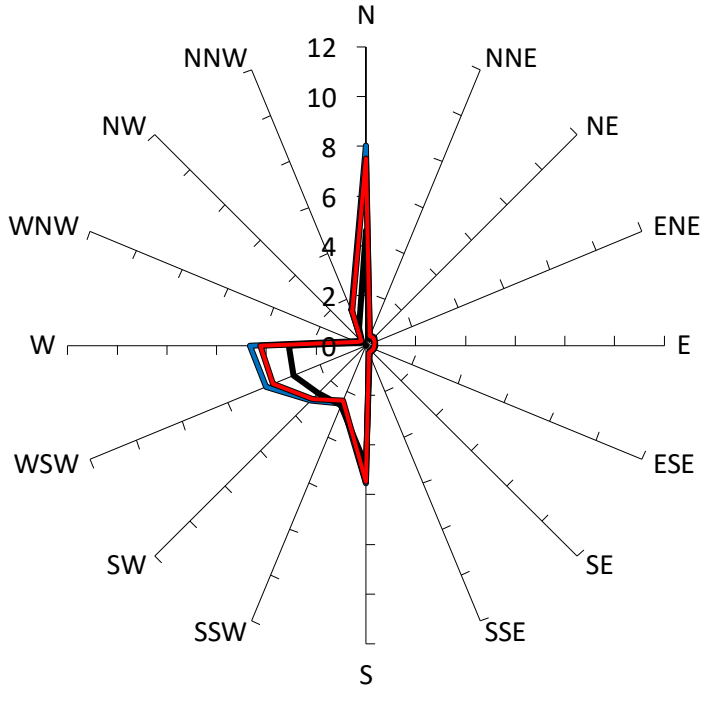


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	6%	14
Existing Site Conditions	14%	17
With the inclusion of the mitigation strategy detailed within the report.	5%	14

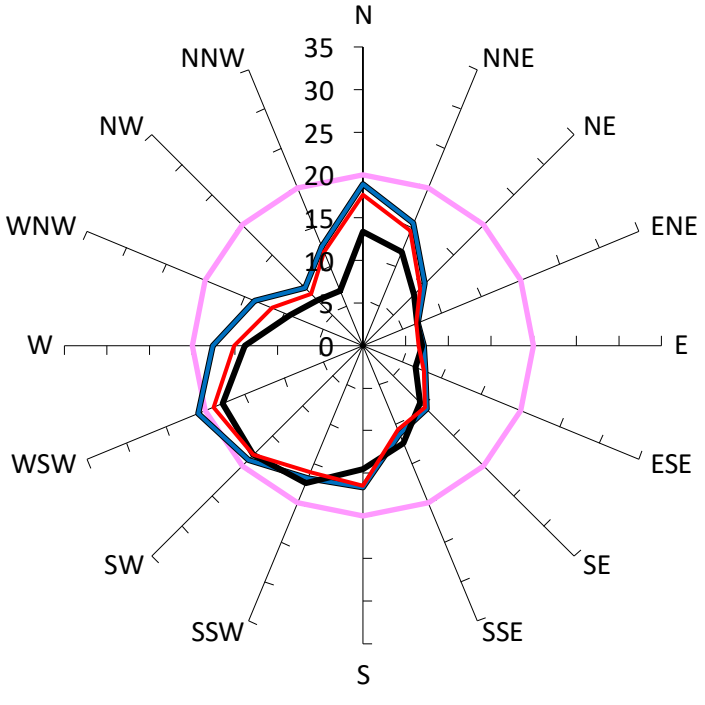
Results for P33

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

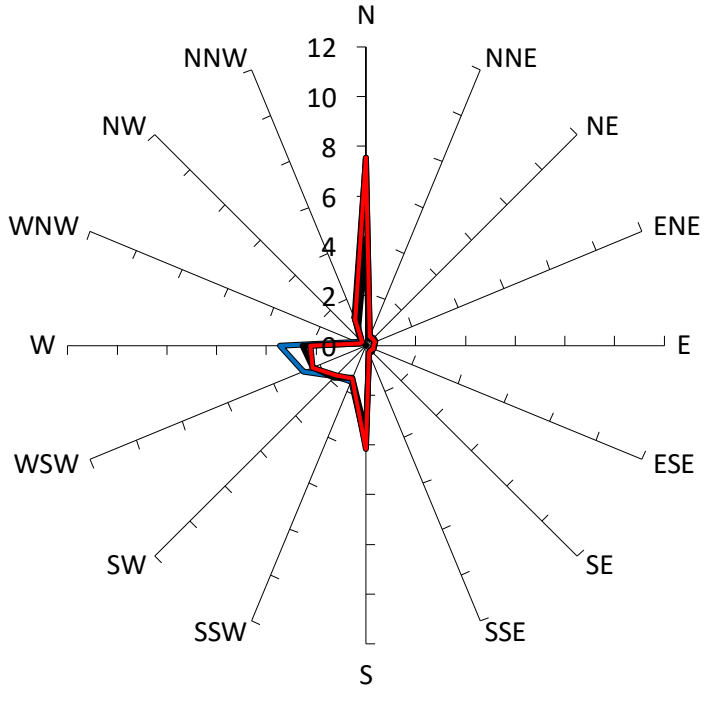


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	33%	21
Existing Site Conditions	15%	18
With the inclusion of the mitigation strategy detailed within the report.	31%	19

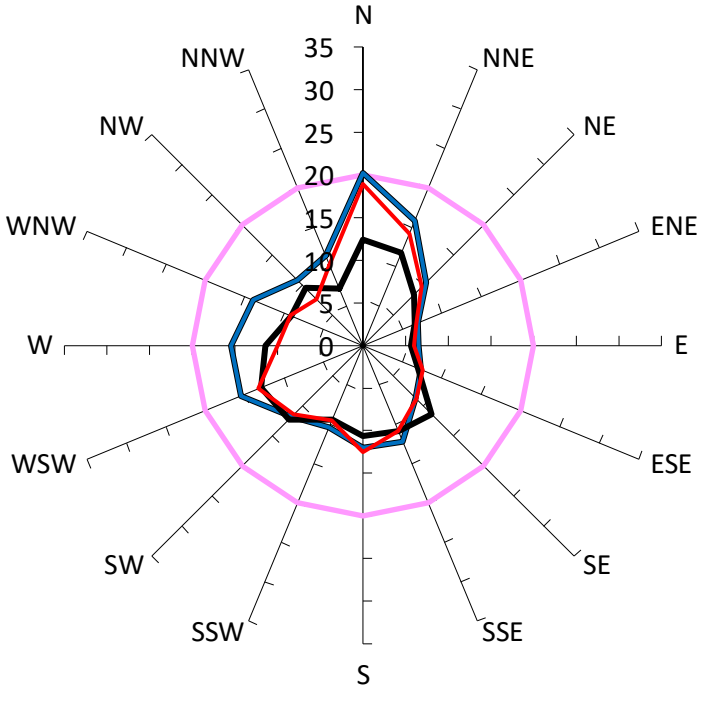
Results for P34

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

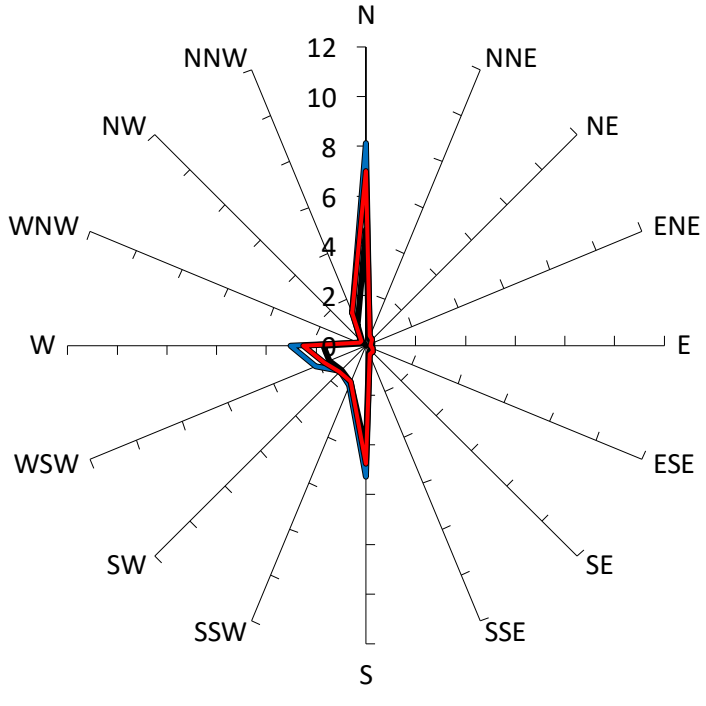


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	19%	20
Existing Site Conditions	5%	13
With the inclusion of the mitigation strategy detailed within the report.	15%	19

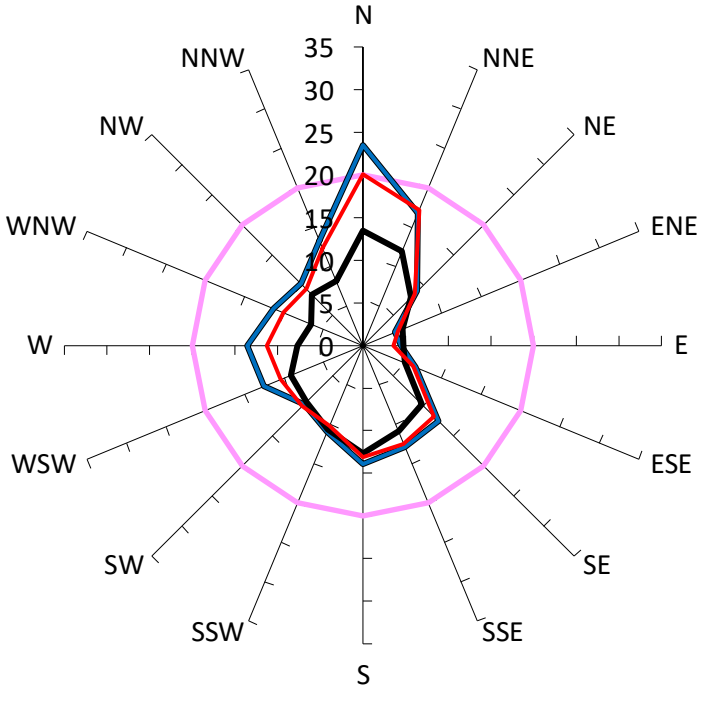
Results for P35

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

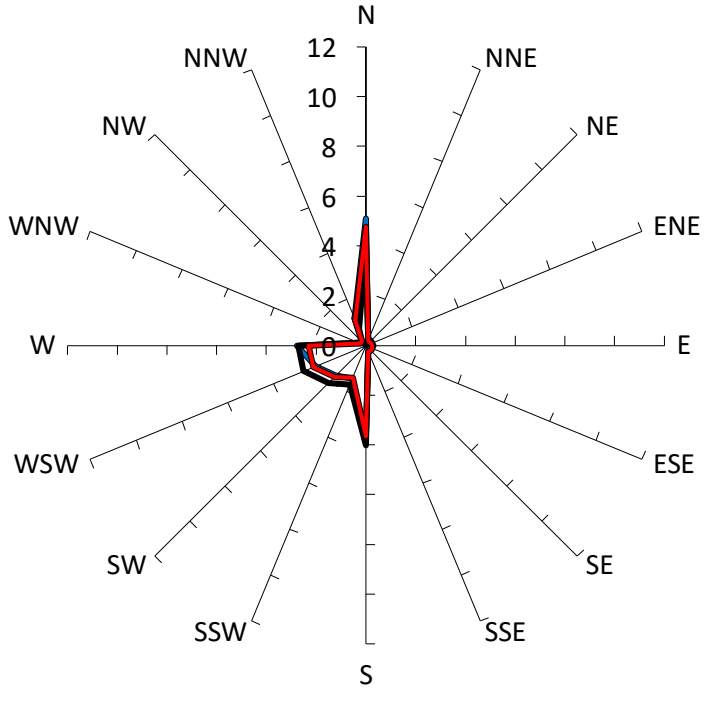


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	21%	23
Existing Site Conditions	5%	13
With the inclusion of the mitigation strategy detailed within the report.	16%	20

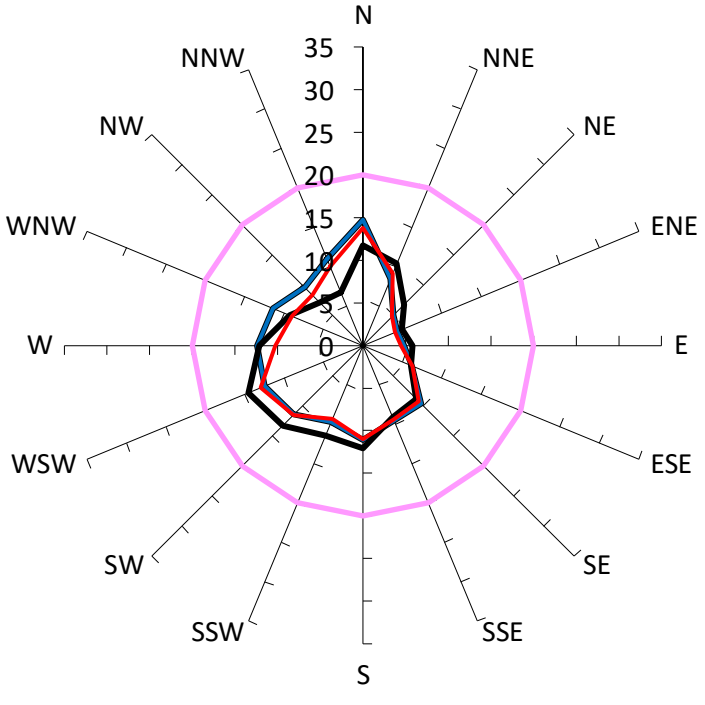
Results for P36

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

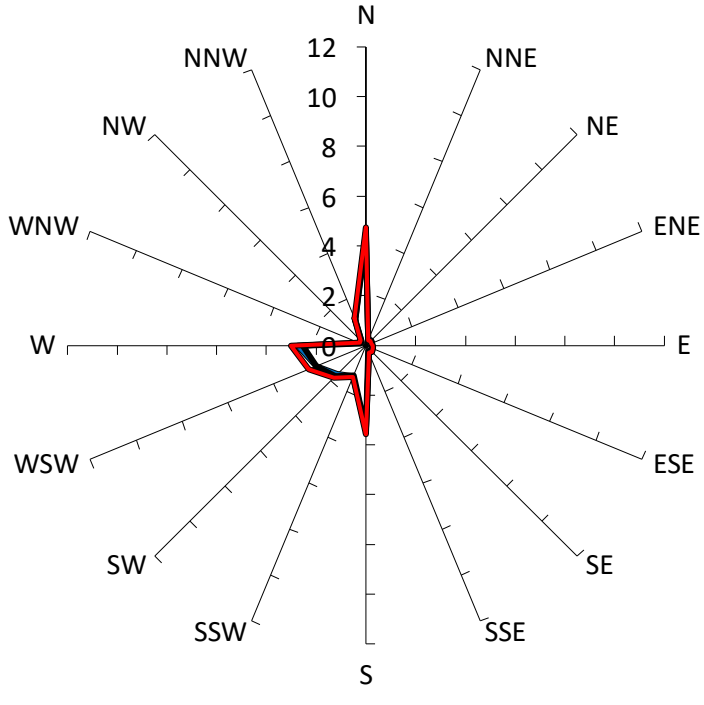


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	8%	15
Existing Site Conditions	6%	15
With the inclusion of the mitigation strategy detailed within the report.	5%	14

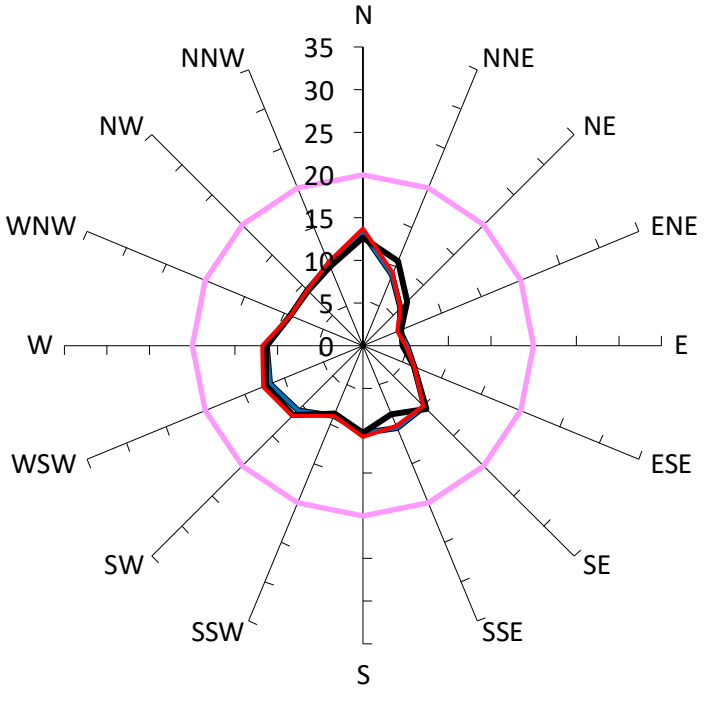
Results for P37

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

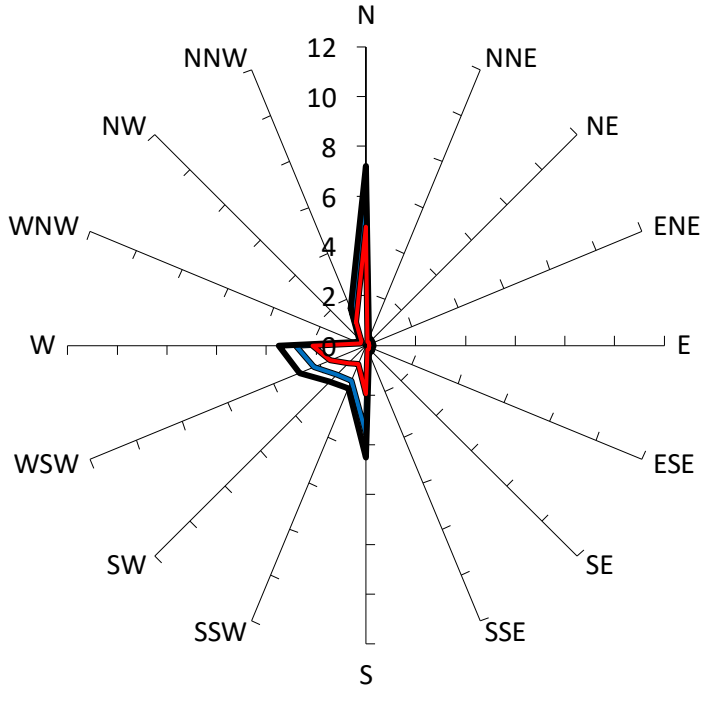


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	5%	13
Existing Site Conditions	4%	13
With the inclusion of the mitigation strategy detailed within the report.	7%	14

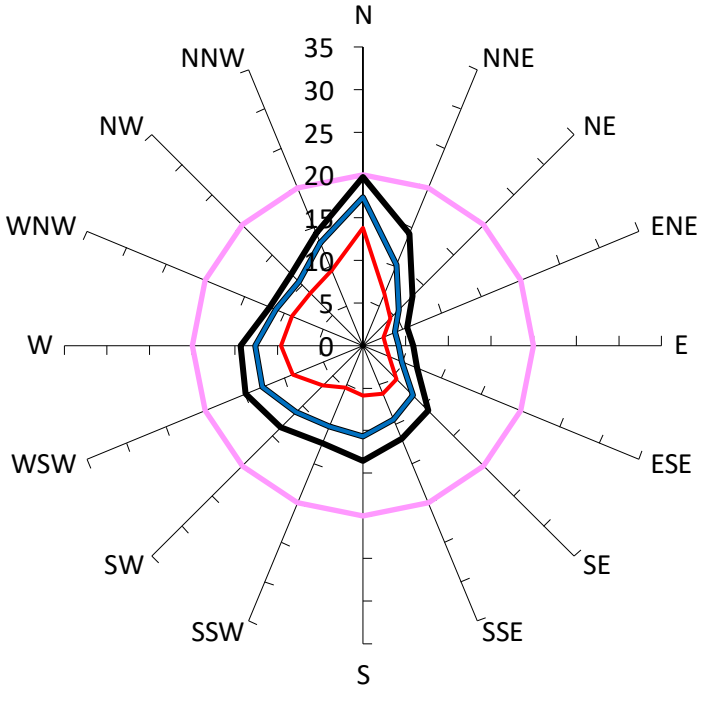
Results for P38

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

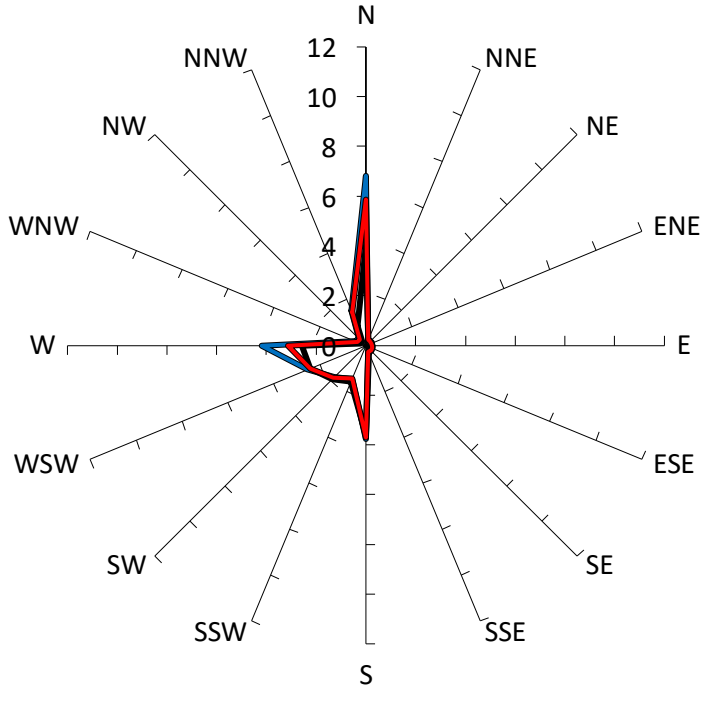


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	12%	17
Existing Site Conditions	22%	20
With the inclusion of the mitigation strategy detailed within the report.	4%	14

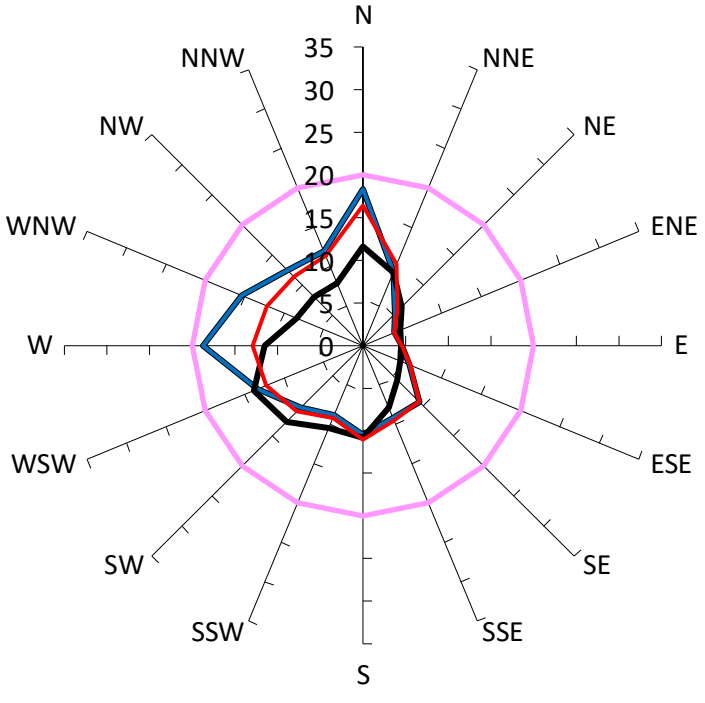
Results for P39

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

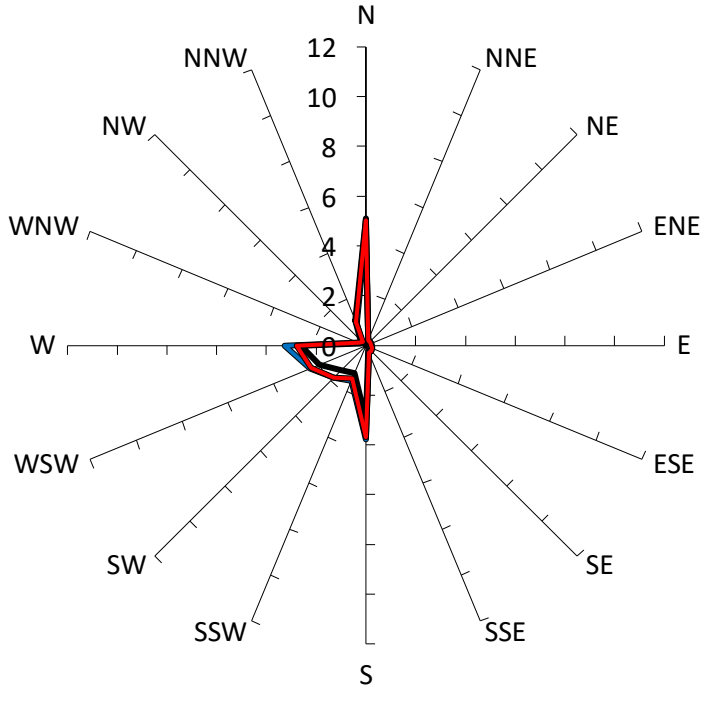


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	21%	19
Existing Site Conditions	4%	14
With the inclusion of the mitigation strategy detailed within the report.	14%	16

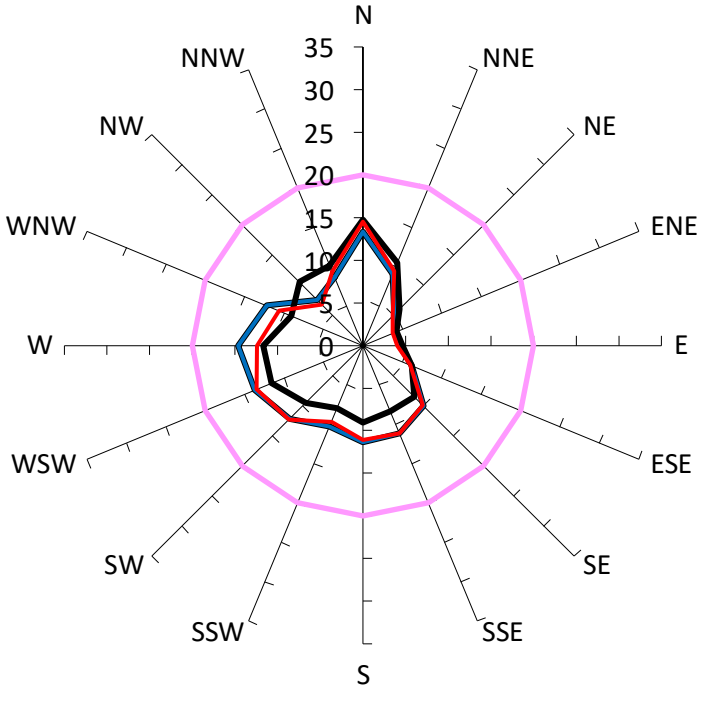
Results for P40

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

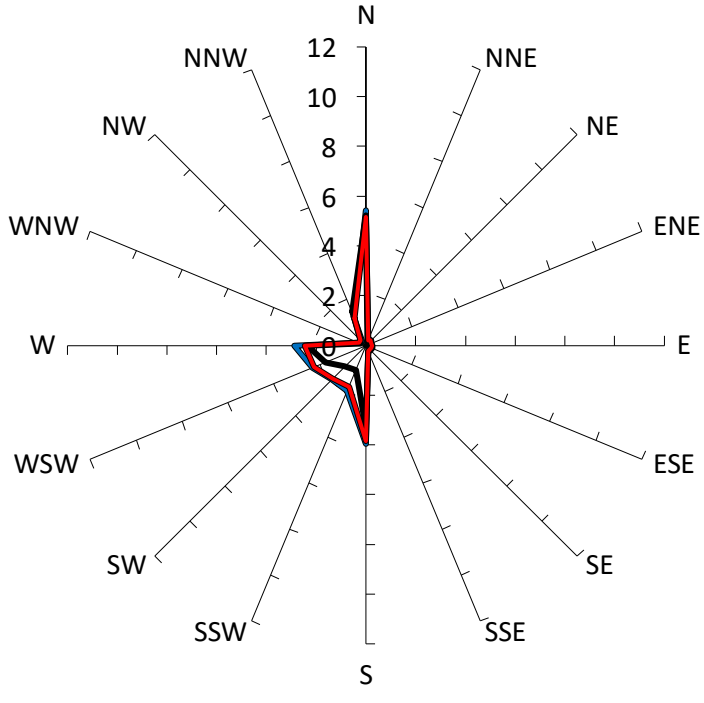


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	7%	15
Existing Site Conditions	7%	15
With the inclusion of the mitigation strategy detailed within the report.	8%	15

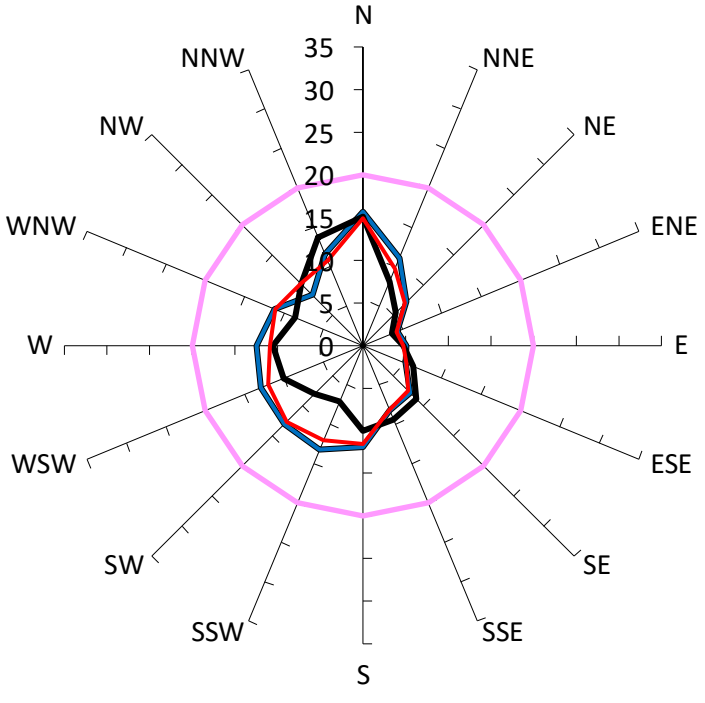
Results for P41

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

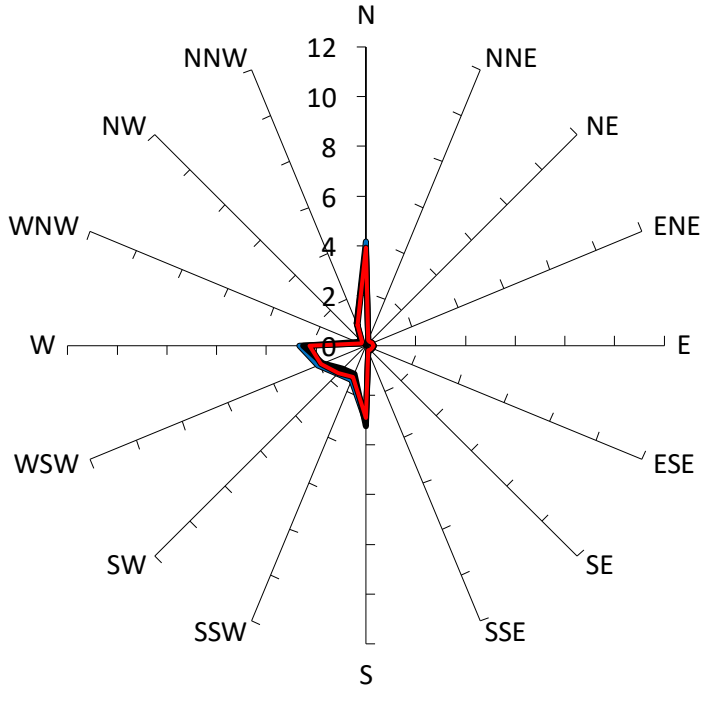


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	12%	16
Existing Site Conditions	8%	15
With the inclusion of the mitigation strategy detailed within the report.	9%	15

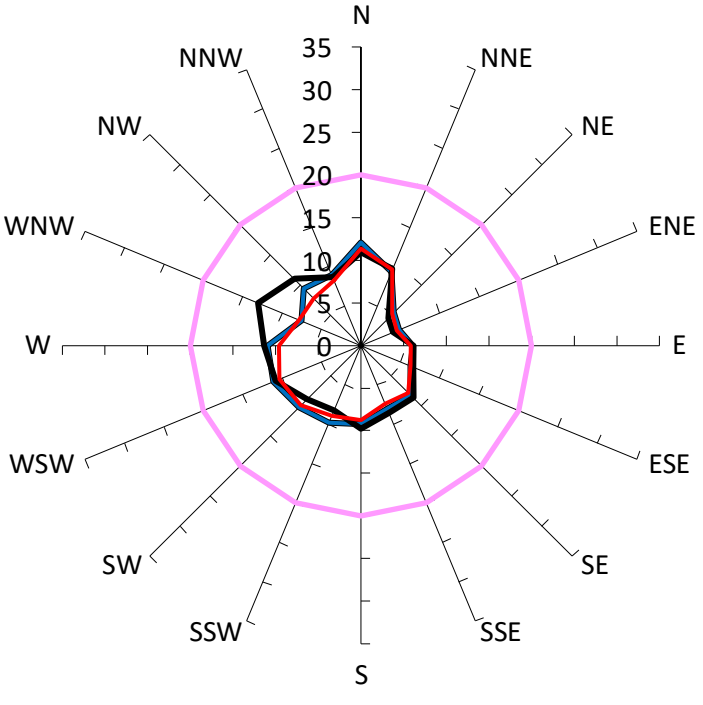
Results for P42

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

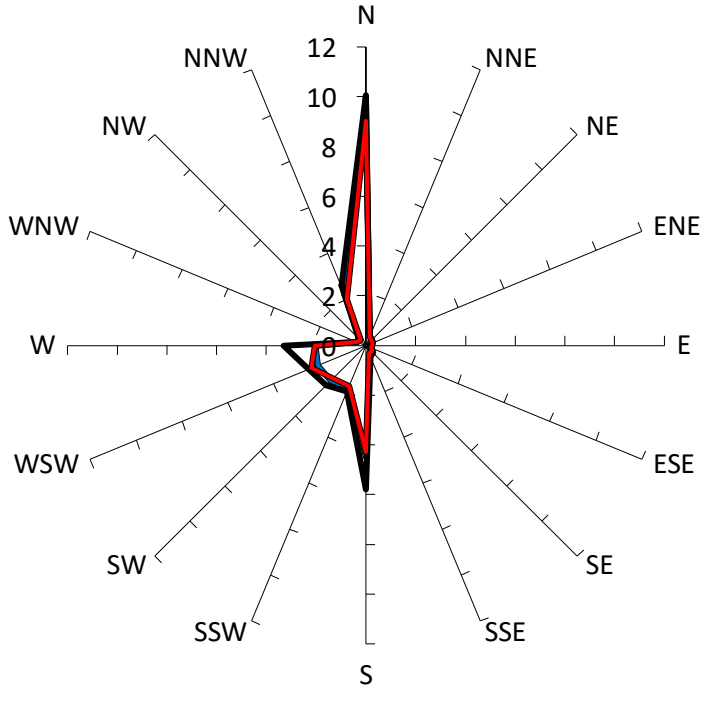


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	3%	12
Existing Site Conditions	3%	13
With the inclusion of the mitigation strategy detailed within the report.	2%	11

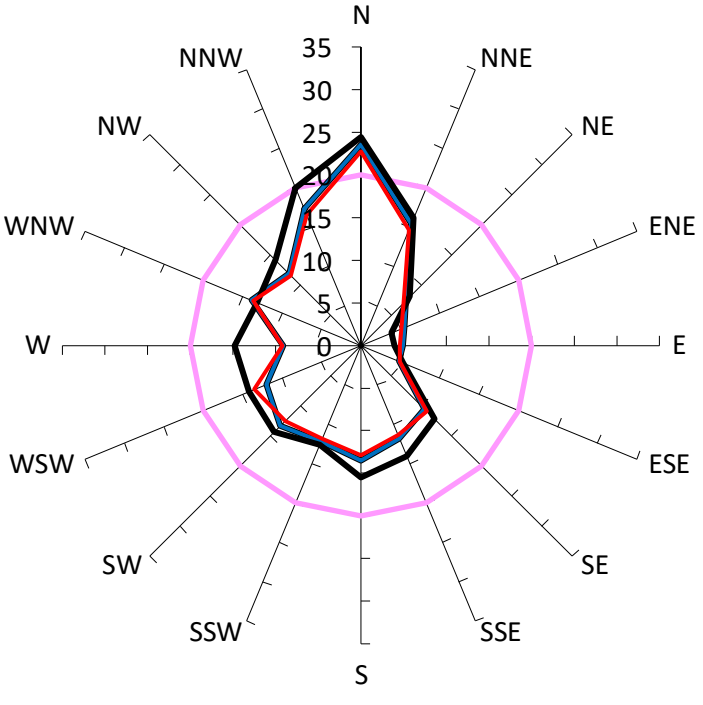
Results for P43

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

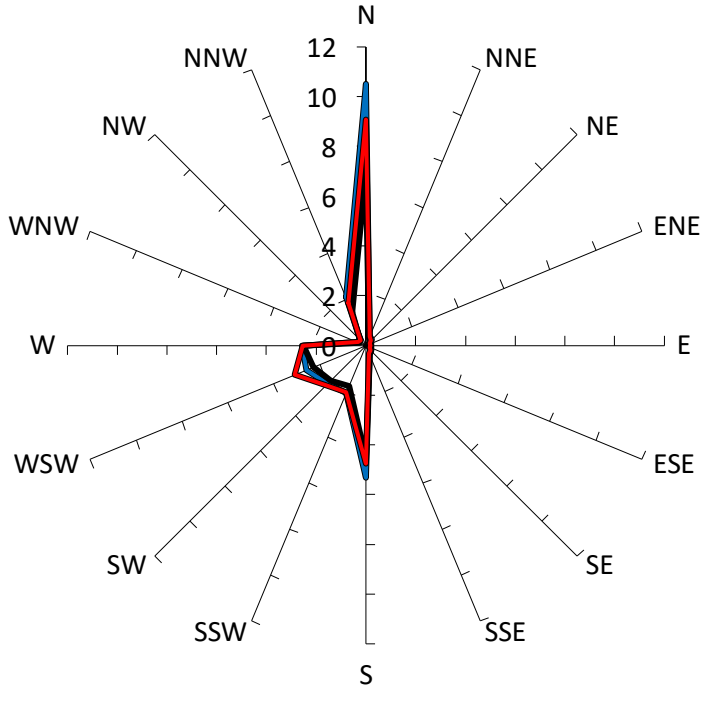


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	22%	24
Existing Site Conditions	31%	24
With the inclusion of the mitigation strategy detailed within the report.	21%	23

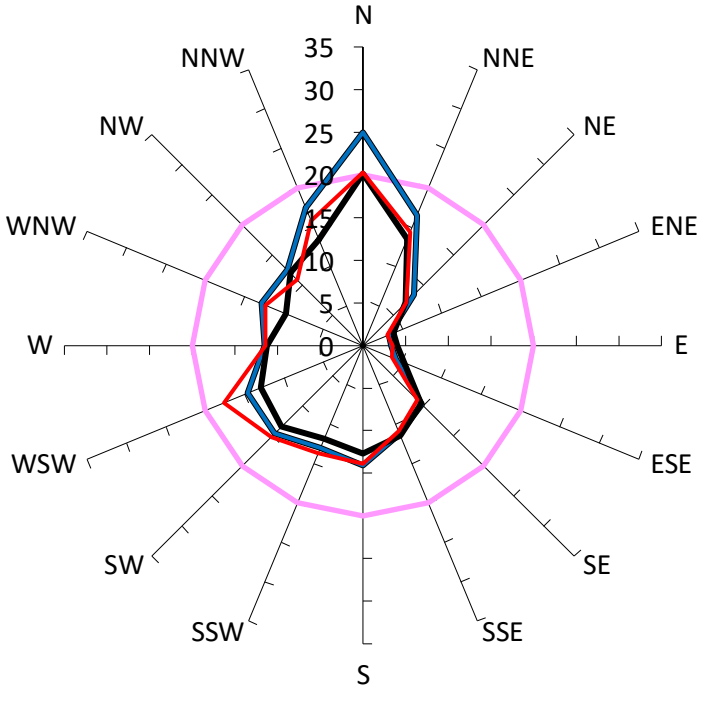
Results for P44

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

Maximum Gust (m/s)

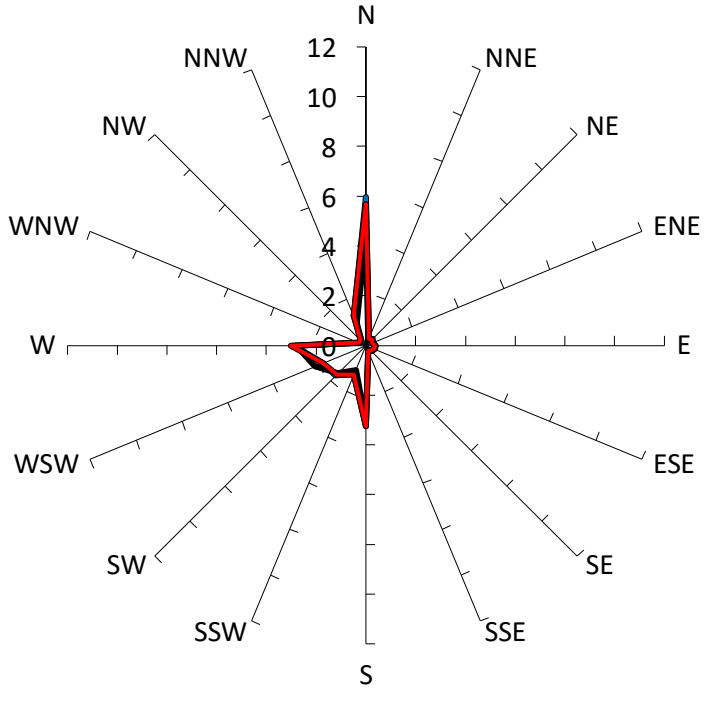


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	26%	25
Existing Site Conditions	16%	20
With the inclusion of the mitigation strategy detailed within the report.	24%	20

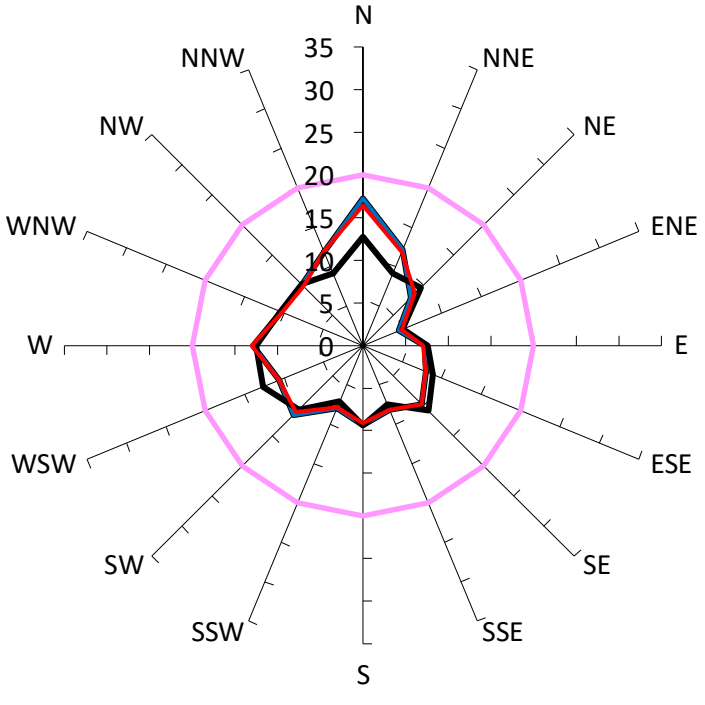
Results for P45

Gust Equivalent Mean (m/s)



Comfort Criteria: 5m/s with 20% probability of exceedence

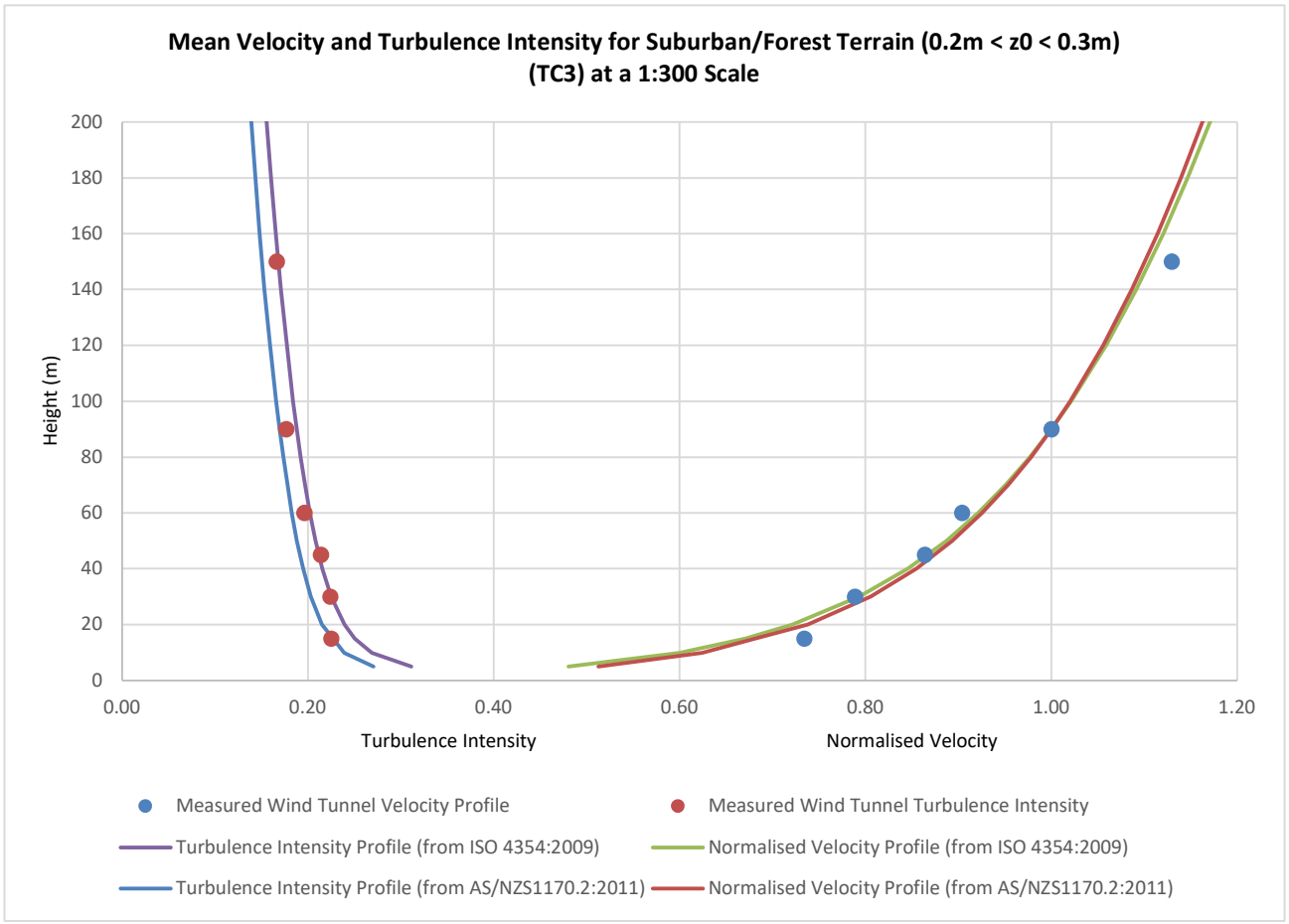
Maximum Gust (m/s)

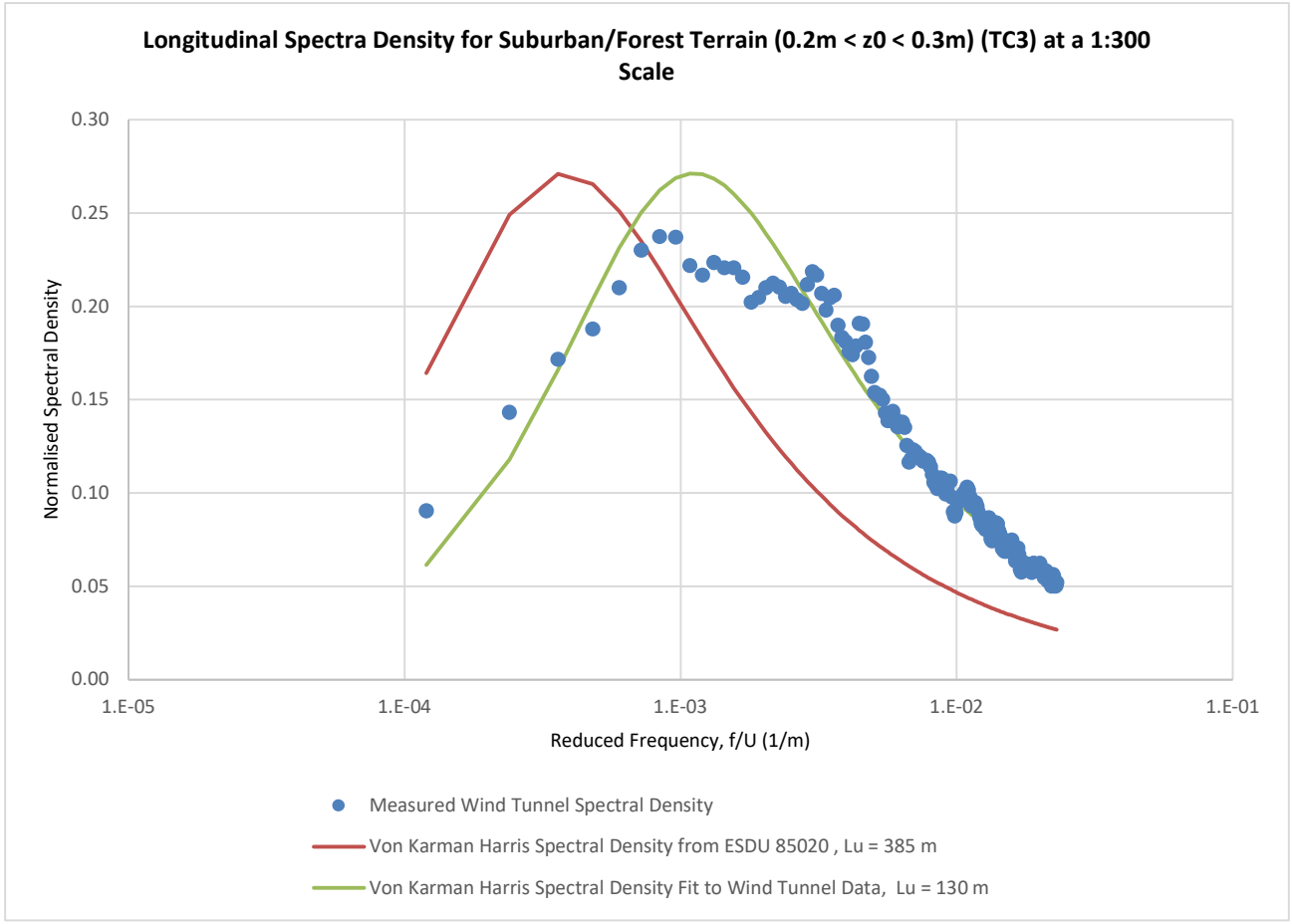


Safety Limit: 20m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
Criterion: Walking comfort (5m/s) Safety Limit (23m/s).	20%	20
With development "as proposed", no vegetation or other treatments.	12%	17
Existing Site Conditions	5%	13
With the inclusion of the mitigation strategy detailed within the report.	12%	16

APPENDIX D VELOCITY AND TURBULENCE INTENSITY PROFILES


Mean Velocity and Turbulence Intensity for Suburban/Forest Terrain (0.2m < z0 < 0.3m) (TC3) at a 1:300 Scale
Height (m)
200
180
160
140
120
100
80
60
40
20
0
0.00
0.20
0.40
0.60
0.80
1.00
1.20
Turbulence Intensity
Normalised Velocity
Measured Wind Tunnel Velocity Profile
Measured Wind Tunnel Turbulence Intensity
Turbulence Intensity Profile (from ISO 4354:2009)
Normalised Velocity Profile (from ISO 4354:2009)
Turbulence Intensity Profile (from AS/NZS1170.2:2011)
Normalised Velocity Profile (from AS/NZS1170.2:2011)


Longitudinal Spectra Density for Suburban/Forest Terrain (0.2m < z0 < 0.3m) (TC3) at a 1:300 Scale
Normalised Spectral Density
0.30
0.25
0.20
0.15
0.10
0.05
0.00
1.E-05
1.E-04
1.E-03
1.E-02
1.E-01
Reduced Frequency, f/U (1/m)
Measured Wind Tunnel Spectral Density
Von Karman Harris Spectral Density from ESDU 85020 , Lu = 385 m
Von Karman Harris Spectral Density Fit to Wind Tunnel Data, Lu = 130 m

APPENDIX E IN-PRINCIPLE WIND MITIGATION STRATEGIES TO ADDRESS WIND COMFORT CRITERIA

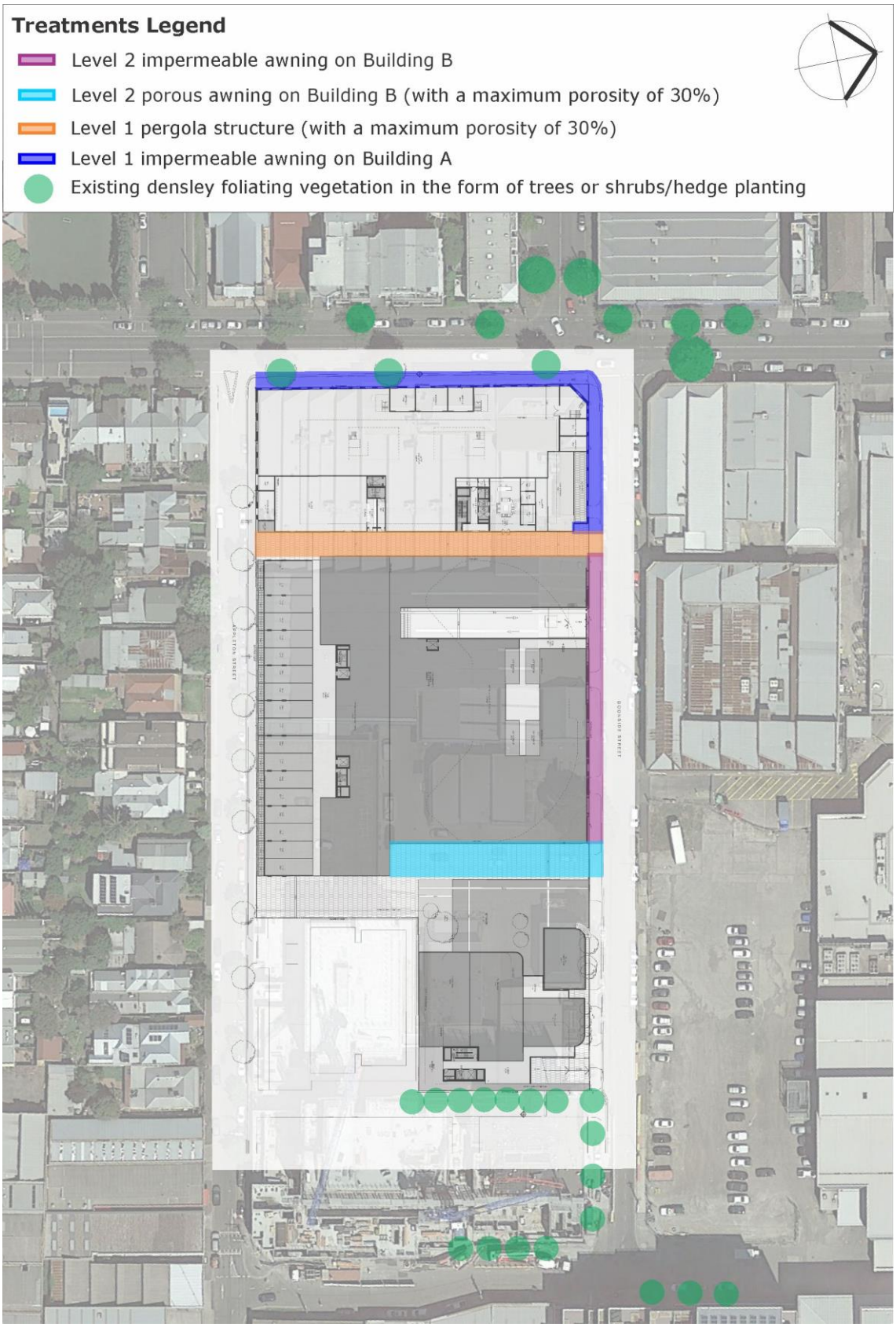


Figure E.1: Suggested Treatments – Overall Ground Level

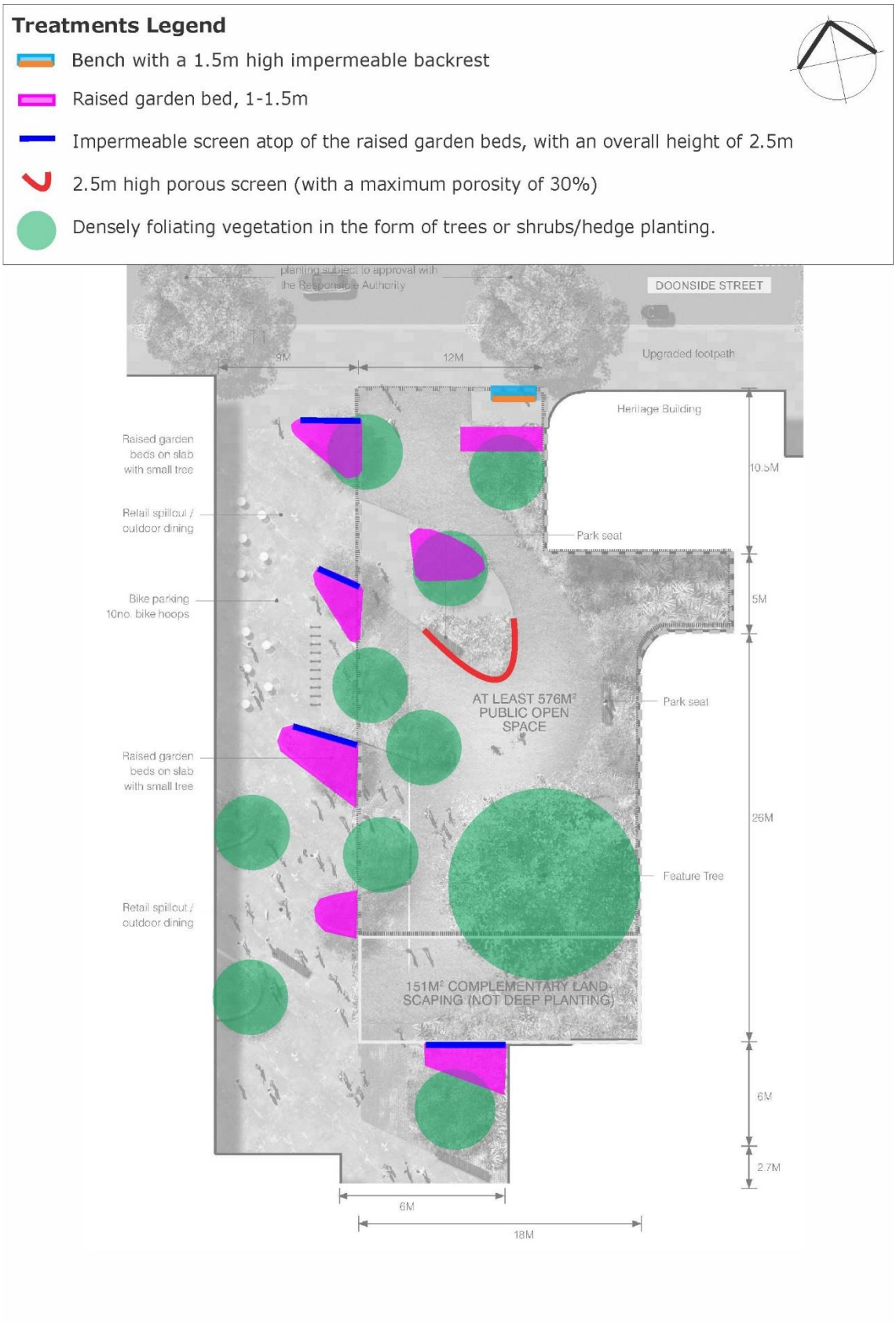


Figure E.2: Suggested Treatments – Doonside Park Communal Open Space